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Published in:

Proceedings of the 17th OptoElectronics and Communications Conference

Link to article, DOI:

[10.1109/OECC.2012.6276694](https://doi.org/10.1109/OECC.2012.6276694)

Publication date:

2012

[Link back to DTU Orbit](#)

Citation (APA):

An, Y., Lorences Riesgo, A., Seoane, J., Ding, Y., Ou, H., & Peucheret, C. (2012). Transmission Property of Directly Modulated Signals Enhanced by a Micro-ring Resonator. In *Proceedings of the 17th OptoElectronics and Communications Conference* (pp. 915-916). IEEE. <https://doi.org/10.1109/OECC.2012.6276694>

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Transmission Property of Directly Modulated Signals Enhanced by a Micro-ring Resonator

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Abstract

A silicon micro-ring resonator is used to enhance the modulation speed of a 10-Gbit/s directly modulated laser to 40 Gbit/s. The generated signal is transmitted error free over 4.5 km SSMF. Dispersion tolerance is also studied.

I. INTRODUCTION

The ubiquitous demand for bandwidth triggered by the introduction of new services such as high-definition video is setting new requirements for short-reach applications, for instance in access and local area networks. For those applications, directly modulated lasers (DMLs) are often preferred over conventional external modulation schemes due to cost, footprint and power consumption constraints. Even though edge-emitting DMLs [1] and vertical-cavity surface-emitting lasers (VCSELs) [2] capable of operating at 40 Gbit/s have been demonstrated, generating and transmitting such high-speed directly-modulated signals error-free, i.e. with a bit-error-ratio (BER) better than 10^{-9} , is still challenging.

Chirped managed lasers (CMLs), where direct modulation is followed by optical filtering rely on the conversion of the adiabatic chirp of the laser to intensity modulation, thereby generating dispersion-tolerant high extinction ratio (ER) signals [3]. Various optical filter technologies have been employed for this purpose, including fibre Bragg gratings, thin-film filters, or delay interferometers. However, these solutions are not always applicable to short range links since such optical filters tend to be bulky and unsuitable for integration.

We have recently proposed and demonstrated a novel transmitter design using a silicon micro-ring resonator (MRR) to enhance the modulation speed of a commercially available 10 Gbit/s DML up to 40 Gbit/s with error-free performance [4]. The transmission of such signals over optical fibres has however not been analyzed yet. In this paper, we report the first study of the transmission performance of directly modulated signals enhanced by an MRR over standard single mode fibre

(SSMF). Error-free transmission with moderate penalty is experimentally demonstrated at 40 Gbit/s over up to 4.5 km SSMF. Numerical studies are furthermore used to discuss the optimum MRR design.

II. EXPERIMENTAL SETUP

As shown in Fig. 1, a commercially available DFB laser diode (NEL), designed for operating at 10 Gbit/s, was directly modulated at 40 Gbit/s with a 2^{11} -1 non return-to-zero (NRZ) pseudo-random binary sequence (PRBS). The DML was biased at 75 mA and modulated with 2.5 V peak-to-peak signal. Such a high bias current allows the adiabatic chip to dominate over the transient chirp. The modulated signal was then coupled to the MRR and collected again via tapered fibres. An erbium-doped fibre amplifier (EDFA) was used to compensate the free-space coupling loss, followed by a 2 nm band-pass filter (BPF) for noise reduction. The filter was chosen to be wide enough to avoid introduction of any extra filtering which could impact the result. The signal was then either connected to the receiver (back-to-back), or launched to a variable length of SSMF. At the end of the link, the signal was received in a pre-amplified optical receiver.

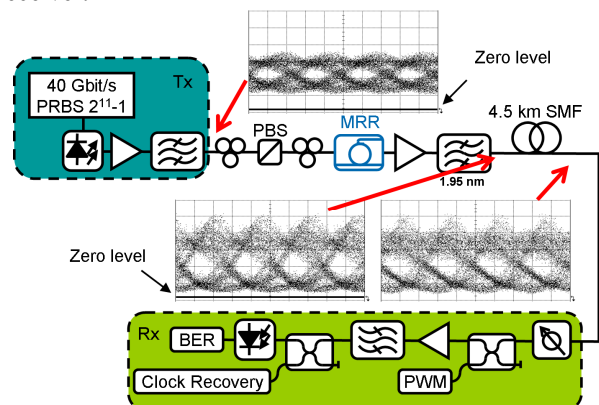


Fig. 1. Experimental setup and eye diagrams before MRR, after MRR and after 4.5 km SSMF transmission

The MRR used in this work was fabricated on a silicon-on-insulator platform by electron-beam lithography followed by reactive ion etching according to the process described in details in [5]. It had a free spectral range (FSR) of 200 GHz, corresponding to the standard wavelength division multiplexing grid and a measured Q-factor of 3300. The through port of the

This work was supported by the 7th framework programme of the European Commission through the “Developing Aircraft Photonic Networks” (DAPHNE, ref. 233709) project, the Danish National Advanced Technology Foundation through the “Self-configurable Optical Links” (ref. 058-2009-3) project and the EURO-FOS (ref. 224402) network of excellence.

resonator was used to filter the DML output spectrum.

III. RESULTS AND DISCUSSIONS

The DML was designed to operate at 10 Gbit/s, where a sensitivity ($\text{BER} = 10^{-9}$) of -30 dBm was measured with a nominal bias of 45 mA, which is a good compromise between a signal affected by relaxation oscillations and associated transient chirp (low bias) and a low extinction ratio (high bias). When operating at 40 Gbit/s with 75 mA bias, an error floor is present, as shown in Fig. 2(b), and the BER is limited to 7.4×10^{-6} at -15 dBm received power. Thanks to the MRR, the BER is improved to 10^{-10} with the same received power. The eye diagram is significantly opened and the “0” level is largely suppressed, at the expense of some overshoot on the “1” level, as can be seen in Fig. 1. The sensitivity at 10^{-9} was about -17.2 dBm and the optimum detuning (detuning of the MRR notch to the long-wavelength side of the DML spectrum, as shown in Fig. 2(a)) was 0.2 nm [4].

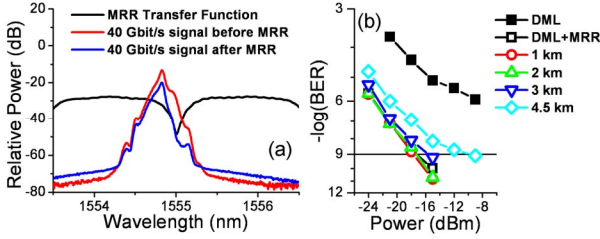


Fig. 2. Experimental results: (a) Signal spectra before and after the MRR and (b) BER performance at the DML output, after the MRR and after different length of SSMFs.

Using the proposed transmitter, the signal was transmitted error free up to 4.5 km SSMF (equivalent to 76.5 ps/nm dispersion) without dispersion compensation, as shown in Fig. 2(b). For transmission up to 3 km, no significant BER penalty was noticed. However, after 4.5 km, an error floor starts appearing.

The tolerance to negative dispersion was also studied by transmitting the signal through different lengths of dispersion compensating fibre (DCF). The sensitivity at 10^{-9} for different amounts of dispersion can be found in Fig. 3(a). The dispersion tolerance is found to be asymmetric with better performance observed for positive dispersion.

In order to interpret those results and study the impact of different MRR designs on the transmission performance, the sensitivity of the signal generated by the proposed transmitter was evaluated numerically as a function of dispersion. The laser parameters were extracted from the DFB laser used in the experiment. The signal generated with 42.8 Gbit/s direct modulation had a 2 dB ER and 12 GHz adiabatic chirp. The MRR parameters can be found in Table I. The MRR used in the experiment was fitted numerically, corresponding to MRR3 in Table I.

The sensitivity was evaluated at $\text{BER} = 10^{-3}$ using Monte Carlo error counting. The numerical results are represented in Fig. 3 (b) and show a good qualitative match with the experimental measurements. From the

simulations it is possible to conclude that the transmission dispersion tolerance is affected by the dispersion of the MRR transfer function. Since the MRR with lower coupling coefficient introduces more positive dispersion to the signal, it results in a reduced dispersion tolerance in the transmission fibre.

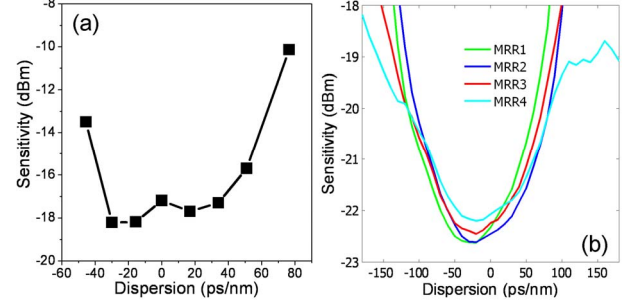


Fig. 3. Dispersion tolerance: (a) Experimental results of sensitivity ($\text{BER} = 10^{-9}$) vs. dispersion. (b) Numerical results of sensitivity ($\text{BER} = 10^{-3}$) vs. dispersion (b).

TABLE I: MRR PARAMETERS

MRR Name	FSG (GHz)	Coupling Coefficient, κ^2 [5]
MRR1	100	0.6
MRR2	100	0.8
MRR3	200	0.6
MRR4	200	0.8

IV. CONCLUSIONS

We have shown that a newly proposed scheme where a silicon MRR is used to enhance the modulation speed of a DML is robust to transmission over SSMF. Transmission of a 40 Gbit/s signal generated using a standard commercially available 10 Gbit/s DFB laser is demonstrated error-free and with moderate penalty up to 4.5 km. The error-free range was experimentally determined to -50 ~ 80 ps/nm dispersion. The influence of the MRR dispersion was clarified using numerical simulations. The proposed scheme can be scaled up to higher bit rates and to multi-channel operation. It can also be straightforwardly adapted to VCSEL sources, resulting in a potential low-cost transmitter for short-reach networks.

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