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Benchmarking state-of-the-art numerical simulation techniques for analyzing large photonic crystal membrane line defect cavities

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ABSTRACT

In this work, we perform numerical studies of two photonic crystal membrane microcavities, a short line-defect L5 cavity with relatively low quality (Q) factor and a longer L9 cavity with high Q . We compute the cavity Q factor and the resonance wavelength λ of the fundamental M1 mode in the two structures using five state-of-the-art computational methods. We study the convergence and the associated numerical uncertainty of Q and λ with respect to the relevant computational parameters for each method. Convergence is not obtained for all the methods, indicating that some are more suitable than others for analyzing photonic crystal line defect cavities.

Keywords: Computational electromagnetic methods, microcavities, photonic crystal, Q factor, optical resonators.

1. INTRODUCTION

An important platform for planar optical integration is the photonic crystal¹ (PhC) membrane platform, where cavities and waveguides may play a key role in realizing compact optical components with classical functionality² such as switches, lasers, and amplifiers or quantum optical functionality such as integrated sources^{3,4} of quantum light. By leaving out a row of holes in an otherwise perfect PhC membrane lattice, a line defect is created in which light may be guided. If the waveguide is terminated at both ends, the finite-length waveguide forms an Ln cavity, where n denotes the length of the cavity. PhC cavities, and resonators more generally, are typically discussed in terms of their *modes* that, for example, show up as peaks in a scattering spectrum. In practical cavities, these peaks are broadened; the cavity mode dissipates power in the PhC and radiates power out of the PhC, as quantified by the corresponding quality (Q) factor proportional to the photon lifetime.⁵ For laser applications, the Q factor governs the onset of lasing, and for cavity quantum electrodynamics applications, it governs the onset of strong coupling. The Q factor thus represents a key parameter in the design of a PhC membrane cavity.⁶

However, the combination of the large size of the PhC Ln cavity and the full 3D nature of the geometry makes the calculation of the cavity Q factor an extremely demanding numerical challenge.⁷ No matter which numerical method is used, careful convergence checks⁷ with respect to the degrees of freedom must be made.

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In this work, we focus on two structures, a low- Q L5 cavity and a high- Q L9 cavity. We employ the following five different computational methods⁷ to compute the cavity Q factor and the resonance wavelength λ for both structures:

- The finite-difference time-domain (**FDTD**) technique.
- The finite-difference frequency-domain (**FDFD**) technique.
- Three variations of the finite-element method (FEM):
 - An eigenvalue analysis based on JCMSuite (**pFEM**).
 - A scattering analysis based on JCMSuite (**sFEM**).
 - An eigenvalue analysis based on COMSOL (**tFEM**).
- The Fourier modal method (**FMM**).
- The surface integral equation (**SIE**) approach.

For each method, the relevant computational parameters are systematically varied to quantify the numerical error.

2. PHOTONIC CRYSTAL MEMBRANE LINE DEFECT CAVITIES

We consider a finite-size semiconductor PhC membrane geometry illustrated in Fig. 1.⁷ The structure is perforated by an in-plane triangular lattice of circular air cylinders and is surrounded by free space on all sides. The boundary of the structure is chosen such that the boundary cylinders are half circles as shown in Fig. 1. For the semiconductor material, we choose indium phosphide (InP) that is also used in experiments with PhC membranes.⁸

According to MPB simulations,⁹ the periodic PhC structure exhibits a partial bandgap in the plane in the frequency range from 1372 to 1594 nm, and by removing n air holes centrally in the structure, an L_n cavity

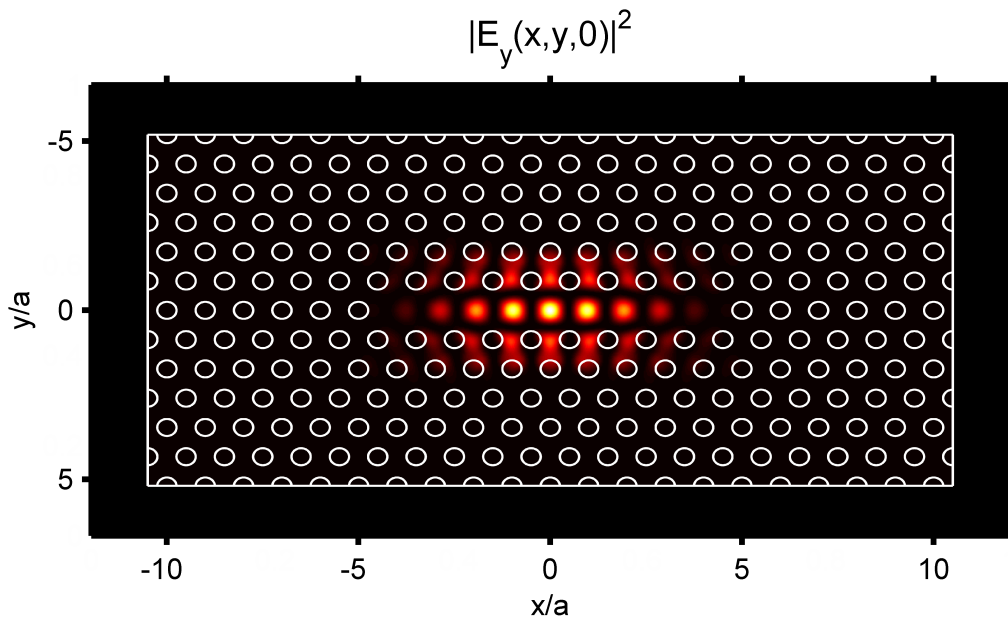


Figure 1. The PhC membrane L9 geometry (white overlay) and the electric field E_y intensity profile for the M1 mode.

is formed. For two lengths of the cavity, $n = 5$ and 9 , we determine the wavelength and Q factor of the fundamental mode in these cavities, the so-called M1 cavity mode, as function of computational parameters. Structural parameters are given in Ref. 7, and we stress that the surrounding air region is, in principle, of infinite extent.

The electric field profile of the fundamental M1 mode in the L9 cavity calculated with FMM is shown in Fig. 1, and the mode features an $|E_y|$ maximum at the center of the geometry. It is noted from Fig. 1 that the mode extends well outside the cavity. For all five numerical methods, we verify qualitatively, by visual inspection, that the calculated modes have this field distribution. In this work, we focus on the convergence of λ and Q for the L5 and L9 configurations described in Ref. 7.

3. NUMERICAL RESULTS

While all methods employ an increasing number of degrees of freedom to provide a more accurate representation of the geometry and thus a more precise estimate of λ and Q , the computational parameters used to describe the degrees of freedom vary greatly for the five methods. To enable comparison of the results in spite of the different parameters used by the methods, we thus present the results as function of a *common geometrical setup index* j .⁷ The exact parameters for the geometrical setup indices for each method are presented in Appendix A, but different values of j for FDTD and FMM, for example, correspond to different mesh sizes and Fourier truncations, respectively. Setup 1 contains the lowest number of degrees of freedom and the setup 8 the highest, and convergence for increasing setup index is thus expected. We use the term *resolution* broadly to discuss the performance of the methods when the number of degrees of freedom is varied.

3.1 Smaller structure and shorter cavity (L5)

We initially focus on the shorter L5 cavity with in-plane PhC dimensions given in Ref. 7. For each of the five numerical techniques, we present calculations of the M1 wavelength and Q factor as function of relevant computational parameters.

In Fig. 2(a) we study the M1 resonance wavelength λ as function of the resolution. The wavelength for the FDTD, pFEM, sFEM, tFEM and SIE methods converges fairly quickly towards a value of $\simeq 1571$ nm. While the wavelength computed using the FDFD method converges more slowly, the final value is similar to that computed using the other methods. However, the wavelength for the FMM increases uniformly indicating that convergence has not been obtained.

The calculated Q factor is presented in Fig. 2(b). Again the pFEM, sFEM, tFEM and SIE methods converge rapidly to values of $\simeq 1710$, whereas the FDTD method converges towards a value of 1687. Large variations are

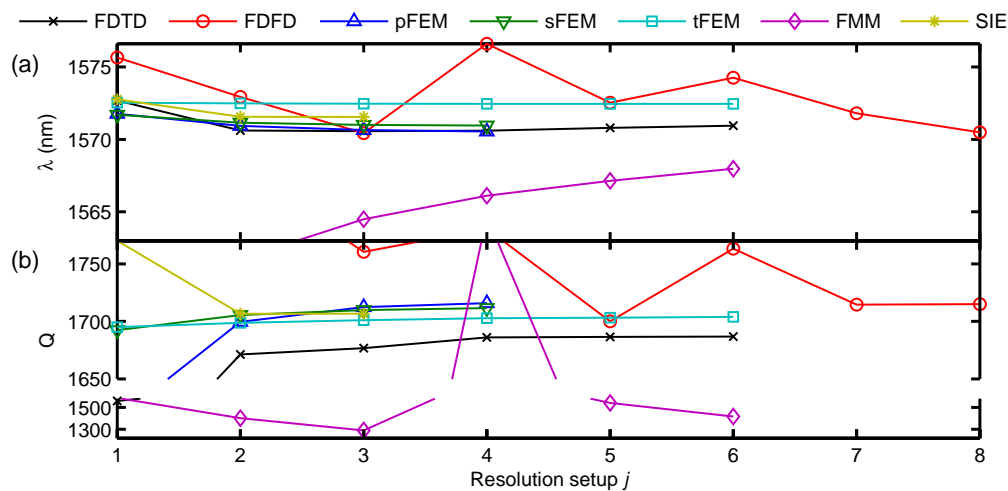


Figure 2. L5: (a) Resonance wavelength λ and (b) Q factor. Notice the disconnected y axis in (b).

again observed for the FDFD technique, which finally converges towards a value similar to that of the pFEM, sFEM, tFEM and SIE methods. The FMM results feature the strongest variations and no clear convergence with a final Q factor of 1417 representing a $\simeq 20\%$ error compared to the other methods.

3.2 Larger structure and longer cavity (L9)

We now consider a longer L9 cavity that is expected to exhibit a higher Q factor than the shorter cavity considered in the previous section. Also, the length and width of the PhC membrane are larger. As for the L5 cavity, we study the resonance wavelength and the Q factor as function of the resolution setup.

The resonance wavelength λ of the L9 cavity is presented in Figs. 3(a) as function of resolution setup. The overall behavior resembles that of the L5 cavity, the wavelength for the FDTD, the FEM and the SIE methods converges rapidly whereas the FDFD results display some variations. The FDTD, the FDFD, the FEM and the SIE methods produce similar wavelengths of $\simeq 1578$ nm. In contrast, the final wavelength computed using FMM is 6 nm smaller, providing a first indication that the FMM has significant difficulty in handling the large L9 cavity.

Results for the Q factor are presented in Figs. 3(b). The Q factor from the FDTD, the FEM and the SIE methods converges towards $\simeq 104,000$. Both the FDFD and the FMM methods display large variations, but whereas the FDFD results appear to converge slowly towards the value predicted by the other methods, the Q factor for the FMM oscillates around an average value of $\approx 25,000$ and thus deviates by almost a factor of 4 from all other results. The FMM thus appears as the least suitable method for handling the large L9 cavity.

4. DISCUSSION

The differences in the Q factors and the resonance wavelengths obtained by the methods indicate that all methods have produced results deviating from the true ones to a larger or lesser degree.⁷ While differences might be expected due to the use of different methods, our benchmark study of the 3 FEMs indicate that deviations occur even for different implementations of the same method.

In our study, independent simulations were performed by the different groups involved in this work using the computational hardware available to each group. In principle, this procedure minimizes the risk of systematic error, and the quantitative agreement may be regarded as more convincing as it has been reached independently. However, it does also mean that in the comparison we should keep in mind that different computational resources were available in the benchmarking of each method. Thus, while the change in computation time with the

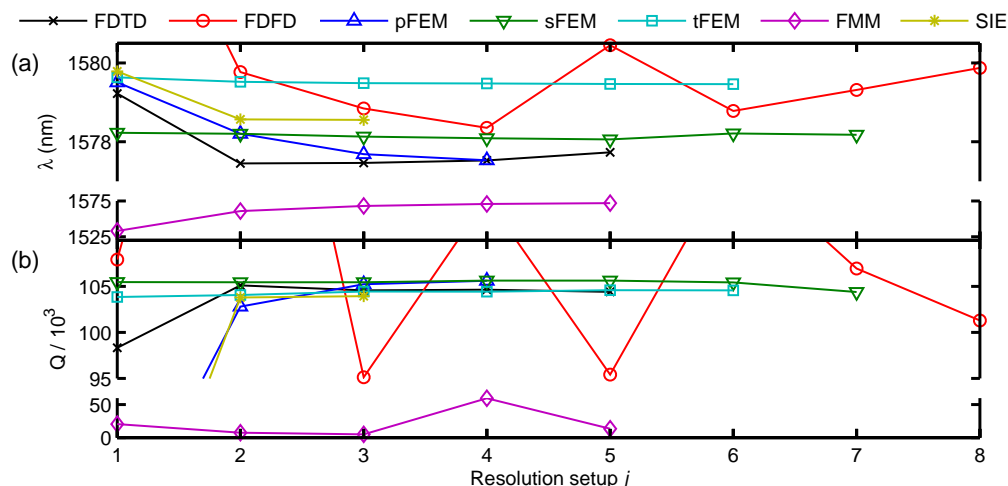


Figure 3. L9: (a) Resonance wavelength λ and (b) Q factor as function of resolution setup. Notice the disconnected y axis.

resolution setup can thus be compared for each method individually, when comparing the computation time for the various methods one should keep in mind that different CPUs with varying clock frequencies were used.

Keeping these differences in available resources in mind, our study⁷ clearly indicates that the least suitable method for analyzing these large PhC line defect cavities is the FMM. The FMM is based on plane-wave expansion of the permittivity profile as well as of the electromagnetic fields, and the poor convergence is likely due to the difficulty of accurately describing the large electric field discontinuities occurring at the InP-air interfaces using this series expansion.¹⁰ On the other hand, these field discontinuities are handled without any problem by the finite difference and finite elements methods which in this respect perform well, but at the cost of significant demands to memory, CPU cores and calculation time. The best performing method in our study is unarguably the SIE approach, which provides excellent convergence using the smallest memory requirement of all the methods.⁷

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Appendix A: Detailed simulation data

The specific numerical parameters represented by the global generalized resolution index j are given in Table 1.

Table 1. Detailed generalized resolution parameters.

Setup #	L5 parameters			L9 parameters		
FDTD	$a/\Delta x$	$a/\Delta y$	$a/\Delta z$	$a/\Delta x$	$a/\Delta y$	$a/\Delta z$
1	13	15	17.5	13	15	17.5
2	26	30	35	26	30	35
3	52	60	70.1	52	60	70.1
4	104	120	140	104	120	140
5	208	240	280	208	240	280
6	438	506	438			
FDFD	$a/\Delta x$	$a/\Delta y$	$a/\Delta z$	$a/\Delta x$	$a/\Delta y$	$a/\Delta z$
1	10.6	10.6	10.6	10.3	10.3	10.3
2	11.5	11.5	11.5	11	11	11
3	12.5	12.5	12.5	11.8	11.8	11.8
4	13.7	13.7	13.7	12.7	12.7	12.7
5	15.2	15.2	15.2	13.7	13.7	13.7
6	16.9	16.9	16.9	14.9	14.9	14.9
7	19.2	19.2	19.2	16.4	16.4	16.4
8	22.2	22.2	22.2	18.2	18.2	18.2
pFEM	p	a/h		p	a/h	
1	2	2.9		2	1.75	
2	3	2.9		3	1.75	
3	4	2.9		4	1.75	
4	5	2.9		5	1.75	
sFEM	p	a/h		p	a/h	
1	2	3.4		3	2.2	
2	3	3.4		3	2.7	
3	4	3.4		3	3.4	
4	5	3.4		3	3.8	
5				3	4.4	
6				3	4.9	
7				3	5.5	
tFEM	p	Min. a/h	Max. a/h	p	Min. a/h	Max. a/h
1	2	1.12	7.6	2	1.12	5.1
2	2	1.12	10.1	2	1.12	7.6
3	2	1.12	15.2	2	1.12	10.1
4	2	1.12	20.3	2	1.12	12.7
5	2	1.12	25.3	2	1.12	15.2
6	2	1.12	30.4	2	1.12	17.7
FMM	l_y	l_z		l_y	l_z	
1	10	7		10	7	
2	20	8		20	8	
3	30	9		30	9	
4	40	10		40	10	
5	50	11		50	11	
6	60	12				
SIE	p_{\max}	g		p_{\max}	g	
1	2	4		2	4	
2	3	4		3	4	
3	4	4		4	4	