Leading edge erosion of wind turbine blades

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Publication date: 2018

Document Version
Peer reviewed version

Citation (APA):
Leading Edge Erosion of Wind Turbine Blades

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Leading Edge Erosion of Wind Turbine Blades

• Wind turbine blades erosion: Reducing the largest uncertainties (EROSION project)

• Extension of the life of blade leading edges by reducing the tip speed during extreme precipitation events

• The meteorological perspectives in rain erosion at leading edges of wind turbine blades
Content

- The EROSION project in brief
- Reducing tip speeds during rain events to extend the life time of blades
- Meteorological perspectives
- Conclusion
The EROSION project in brief

www.rain-erosion.dk
**1. Research hypothesis:** Erosion damage is mainly generated during heavy precipitation (big drops of rain or hail), which occurs in a very little fraction of the turbines operation time. By reducing the tip speed of the blades in these few hours a significant extension of the leading edge lifetime can be obtained with negligible loss of production.

**2. Methodology:** Define rain and hail erosion classes to quantify leading edge blade in-field and in lab testing. Correlations between rain intensity, droplet size, impact speed, materials properties, etc. will be established.

**3. Measurement Device:** Low-cost prototype for precipitation measurement on site and real time warning device enabling modern control of wind turbines.

**4. Erosion safe mode:** A safe mode control based on the erosion classes to control the wind turbine, reducing the tip speed under severe conditions – preventing aerodynamic degradation and reducing maintenance costs.
Rain Erosion Tester by R&D Test Systems

Example of specimen
First results

RET test results for EROSION specimen.
Damage is the first visual damage point of erosion.

3.5 mm droplets
Rain intensity 58 mm/hour

2.4 mm droplets
29 mm/hour

3 (4) different velocities
3 blades

Stop frequently and map the new point damages each time
First results

![Graph showing kinetic energy vs. impacts to failure for different droplet sizes, with equations for the relationship between kinetic energy and impacts to failure.]

- 3.5 mm droplets
  - Equation: $N = 722 \times S^{-1.63}$
  - 95% confidence interval
- 2.4 mm droplets
  - Equation: $N = 16 \times S^{-2.66}$
  - 95% confidence interval
Rain erosion test samples with different degradation have been investigated by electron microscopy.

The erosion appears to start at the surface where the surface roughness increase. However at the same time as the top-coating and the filler slowly degrades microscale damage can be observed within the laminate. Cracks have been observed at the position of the peel fly as well as within the laminate.

Electron microscopy provide a snapshot of the degradation in a polished cross section.
Rain erosion specimen testing map

EROSION test campaign

Leading edge configurations

"conventional coating"

LEP

Filler

Layer thicknesses

v1, v2, v3, v4, v5

d1, d2, d3

droplet size

test parameters

Test parameters

Characterisation

Pre test

US

X CT

X CT

US

SEM

Light Microscopy

Failure modes

surface cracks

debonding of layers

crushing of filler

sub surface cracks

X CT: X-ray Computed Tomography

US: Ultrasonic Scanning

SEM: Scanning Electron Microscopy

DTU Wind Energy, Technical University of Denmark
Extending the life of wind turbine blade leading edges by reducing the tip speed during extreme precipitation events

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Rain erosion test data plotted as a Wöhler curve
Rain erosion test data plotted as a Wöhler curve: Impacts per unit area to failure as function of the kinetic energy for each impact

\[ E_k = \frac{1}{12} \rho \pi D^3 v_t^2 \ [\text{J}] \]
Wöhler curves for droplet diameters of 1.5, 2.0 and 2.5 mm
Control of turbine

Power = Torque * Rotational_Speed
Erosion safe-mode

In an erosion-safe mode the turbine would be downrated meaning that it would act as its rated power was lower than default. That would effectively decrease the rated RPMs.

Power = Torque * Rotational_Speed
Apart from a reference case where it is assumed that there is no erosion, six different control strategies are investigated based on the model for expected lifetime for the blade leading edge:

- Control strategy 1 with expected life time of 1.6 years
- Control strategy 2 with expected life time of 10.4 years
- Control strategy 3 with expected life time of 24.4 years
- Control strategy 4 with expected life time of 53.9 years
- Control strategy 5 with expected life time of 106.5 years
- Control strategy 6 with expected life time of infinite many years
Calculation of the life time of the blade leading edge with no reduction of the tip speed. Control strategy 1

<table>
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<tr>
<th>Rain intensity [mm/hr]</th>
<th>Droplet size [mm]</th>
<th>Percent of time [%]</th>
<th>Hours pr year [hrs/year]</th>
<th>Blade tip speed [m/s]</th>
<th>Hours to failure [hrs]</th>
<th>Fraction of life spent pr year [%]</th>
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Sum of fractions [%]: 64

Expected life [years]: 1.6
Calculation of the life time of the blade leading edge with reduction of the tip speed to 70m/s and 80m/s, respectively: Control strategy 2

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Sum of fractions [%]: 9.6

Expected life [years]: 10.4
Calculation of the life time of the blade leading edge with reduction of the tip speed to 55m/s, 65m/s and 70m/s, respectively: Control strategy 5

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Sum of fractions [%]: 0.9

Expected life [years]: 107
Simulated power curves for the Vestas V52 for different leading edge roughness levels
Simulated power curves for the Vestas V52 for different maximum tip speeds
Cost of operation and maintenance

- Energy price:
  - 50 €/MWh
  - 250 €/MWh
- Inspection cost:
  - 500 €/rotor
  - 1500 €/rotor
- Repair cost:
  - 10000 €/rotor
  - 20000 €/rotor
- Control strategy 1: 10 inspections and 9 repairs
- Control strategy 2: 10 inspections and 1 repairs
- Control strategy 3: 5 inspections and 0 repairs
- Control strategy 4: 5 inspections and 0 repairs
- Control strategy 5: 2 inspections and 0 repairs
- Control strategy 6: 2 inspections and 0 repairs

Stand still of 1 day inspected
Stand still of 2 days repaired
AEP relative to AEP with no erosion

[Bar chart showing AEP relative to reference for different control strategies and wind speeds (A=7m/s, A=8m/s, A=9m/s).]
Loss of income due to erosion, inspection and repair

[Diagram showing loss in income relative to reference for different control strategies and wind speeds (A=7m/s, A=8m/s, A=9m/s).]

Meteorological perspectives
Raindrop size distribution through a horizontal plane with the rain fall intensity as a parameter (from Kubilay et al., 2013, based on Best, 1950)
Average rainfall rate-frequency relationships for four rain climates (Jones and Sims, 1978) ©American Meteorological Society. Used with permission.
Meteorological observation instruments
EROSION disdrometer network

[Map showing various locations and markers such as DMI, DTU-Risø, LM Wind Power, and Aalborg University.]
Size-Velocity histogram for year 2012 to 2017 at Voulund
DMI’s weather radar network shown with an example from 6 June 2017 at 15:20 UTC. The unit dBZ indicates the relative rain rate.
Radar QPE (quantitative precipitation estimate) field on 16 June 2016 at 0900 UTC versus raingauge at Vejle Pumpestation.
Annual rain in Denmark

The average yearly precipitation in Denmark in the reference period 1961-1990 measured in mm.

Annual rain offshore

At offshore sites there are no rain gauges thus approximation and/or extrapolation is necessary.

The new offshore disdrometer data may prove useful for radar-based rain mapping offshore.
Conclusions

The extension of blade life time using erosion safe mode is calculated based on assumptions on erosion related to rain events.

The erosion safe mode control strategy is outlined and the expected reduction in operational cost is estimated.

First tests in rain erosion tester have been completed and preliminary results on damage in specimen are available.

Precipitation data will be collected during next one year.