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H∞ Control of a Wind Turbine

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1 Introduction
Due to recent concerns on global warming and increase in the price of fossil fuel, there has been an increasing interest in green energies of which wind energy is one of the most important ones. Wind turbines are the most common wind energy conversion systems (WECS) and are hoped to be able to compete with fossil fuel power plants on the energy price very soon. However this needs better technology to reduce electricity production price. Control can play an essential part in this context because control methods can decrease the cost of energy by keeping the turbine close to its maximum efficiency and increase the captured power and also reduce structural fatigue and therefore increase lifetime of the wind turbine. There are several methods for wind turbine control ranging from classical control methods [1] which are the most used method in real applications to advanced control methods which have been the focus of research in the past few years [2]. Gain scheduling [3], nonlinear control [4], robust control [5], model predictive control [6], µ-Synthesis [7] just to mention a few. Advanced control methods are thought to be the future of wind turbine control as they can employ new generations of sensors on wind turbines (e.g. LIDAR [8]), new generation of actuators (e.g. trailing edge flaps [9]) and also conveniently treat the turbine as a MIMO system. The last feature seems to become more important than before as wind turbines become bigger and more flexible which make decoupling different modes and designing controller for each mode more difficult. The problem of H∞ control of a wind turbine is considered in this work. Using H∞ method a set of controllers are designed based on a 2 degrees of freedom linearized model of a wind turbine. An extended Kalman filter is used to estimate the effective wind speed and the estimated wind speed is used to find the control signals as a convex combination of outputs of the controllers set. The resulting controller is applied on a full complexity simulation model and simulations are performed for stochastic wind speed according to the relevant IEC standard. The wind turbine in this paper is treated as a MIMO system with pitch (θ) and generator reaction torque (Qg) as inputs and rotor rotational speed (ωr), generator rotational speed (ωg) and generated power (Pω) as outputs. This paper is organized as follows: In the section 2 modeling of the wind turbine including modeling for wind speed estimation and simulation model are addressed. In the section 3 controller design is explain. And finally in the section 4 simulation results are presented.

2 Modeling
For modeling purposes, the whole wind turbine can be divided into 4 subsystems: Aerodynamics subsystem, structural subsystem, electrical subsystem and actuator subsystem. The dominant dynamics of the wind turbine come from its flexible structure. Several degrees of freedom could be considered to model the flexible structure, but for control design mostly just a few important degrees of freedom are considered. In this work we only consider two degrees of freedom, namely the rotational degree of freedom (DOF) and drivetrain torsion, the other parts of the dynamics are considered as uncertainties and is handled by a robust approach.

2.1 Modeling for Wind Speed Estimation
Wind can be modeled as a complicated nonlinear stochastic process, however for practical purposes it could be approximated by a linear model [10]. In this model the wind has two elements, mean value term (vm) and turbulent term (vt):

\[ v_e = v_m + v_t \]

The turbulent term could be modeled by the following transfer function:

\[ v_t = \frac{k(v_m)}{(p_1(v_m)s + 1)(p_2(v_m)s + 1)} e; \quad e \in N(0,1) \]

And in the state space form:

\[
\begin{pmatrix}
\dot{v}_t \\
\dot{v}_t
\end{pmatrix} =
\begin{pmatrix}
0 & 1 \\
-\frac{k(v_m)}{p_1(v_m)p_2(v_m)} & -\frac{1}{p_1(v_m)p_2(v_m)}
\end{pmatrix}
\begin{pmatrix}
v_t \\
v_t
\end{pmatrix} +
\begin{pmatrix}
0 \\
\frac{k(v_m)}{p_1(v_m)p_2(v_m)}
\end{pmatrix} e
\] (1)

This is a second order approximation of the wind power spectrum [11]. For wind speed estimation, a one DOF nonlinear model of the wind turbine is augmented with the wind model given above. An extended Kalman filter uses this model to estimate the effective wind speed.

\[
\begin{pmatrix}
\dot{v}_t \\
\dot{v}_t
\end{pmatrix} =
\begin{pmatrix}
0 & 1 \\
-\frac{k(v_m)}{p_1(v_m)p_2(v_m)} & -\frac{1}{p_1(v_m)p_2(v_m)}
\end{pmatrix}
\begin{pmatrix}
v_t \\
v_t
\end{pmatrix} +
\begin{pmatrix}
0 \\
\frac{k(v_m)}{p_1(v_m)p_2(v_m)}
\end{pmatrix} e
\]
This wind speed is used to find the operating point of the wind turbine and to calculate appropriate control signals.

2.2 Nonlinear Model

Blade element momentum (BEM) theory [12] is used to calculate aerodynamic torque and thrust on the wind turbine. This theory explains how torque and thrust are calculated on the wind turbine and to calculate appropriate control signals to punish high frequency actions. Also we have setup low pass filters to punish low frequency of the actuators, we have put high pass filter on control signals to punish high frequency actions. Also we have considered the second objective. Control objectives are formulated in the form of weighting functions on input disturbances (d) and exogenous outputs (z) (figure 1). In order to avoid high frequency activity of the actuators, we have put high pass filter on control signals to punish high frequency actions. Also we have setup low pass filters to punish low frequency of some of the system outputs as their high frequency dynamics are outside of our actuator bandwidth and we can not control them. For regulating power and rotational speed, \( \int P_g - P_g^{ref} \) and \( \int \omega_g - \omega_g^{ref} \) and for minimizing fatigue loads on the drivetrain \( \omega_g - N_r \omega_r \) are punished. The resulting controller is a dynamical system with measurements \( y \) as its inputs and control signals \( u \) as its outputs:

\[
\begin{align*}
\dot{x}_c &= A_c x_c + B_c y \\
u &= C_c x_c
\end{align*}
\]

3 Controller Design

3.1 Control Objectives

The most basic control objective of a wind turbine is to maximize captured power and prolong life time of the wind turbine. The second objective is achieved by minimizing the fatigue loads. Generally maximizing power capture is considered in the partial load and minimizing fatigue loads is mainly considered above rated. As we are operating in the full load region in this work, we have considered the second objective. Control objectives are formulated in the form of weighting functions on input disturbances (d) and exogenous outputs (z) (figure 1). In order to avoid high frequency activity of the actuators, we have put high pass filter on control signals to punish high frequency actions. Also we have setup low pass filters to punish low frequency of some of the system outputs as their high frequency dynamics are outside of our actuator bandwidth and we can not control them. For regulating power and rotational speed, \( \int P_g - P_g^{ref} \) and \( \int \omega_g - \omega_g^{ref} \) and for minimizing fatigue loads on the drivetrain \( \omega_g - N_r \omega_r \) are punished. The resulting controller is a dynamical system with measurements \( y \) as its inputs and control signals \( u \) as its outputs:

\[
\begin{align*}
\dot{x}_c &= A_c x_c + B_c y \\
u &= C_c x_c
\end{align*}
\]
controllers are presented. Kaimal model is used as the turbulence model and in order to stay in the full load region, category C of the IEC turbulence categories with 18m/s as the mean wind speed is chosen.

4.1 Wind Speed Estimation
An extended Kalman filter is used to estimate the wind speed. Figure 3 shows the effective and the estimated wind speeds.

5 Conclusion
In this paper we solved the problem of nominal performance control of a wind turbine using $H_{\infty}$ theory. As the wind turbine is a nonlinear system we have linearized the system on a grid of operating points and designed controllers for each linear model. Estimated wind speed is used to calculate control signal from outputs of controllers. The final controller is implemented on a FAST simulation model with 10 degrees of freedom and simulation with stochastic wind speed based on IEC standard is done. The results show good regulation of generated power and rotational speed for a big range of wind speed changes.

Figure 2: Bode plots for performance specifications (y-axis is in dB and x-axis is in rad/s)

Figure 3: Wind speed (blue-solid), Estimated wind speed (red-dashed), unit is m/s

Figure 4: Blade-pitch (degrees)
Figure 5: Generator-torque (N.M.)

Figure 6: Rotational speed (rpm)

Figure 7: Electrical power (mega watts)

References


