Consequences of severe radioactive releases to Nordic Marine environment
Final report for the NKS-B activity 2012

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Consequences of severe radioactive releases to Nordic Marine environment

Iosjpe¹, M., Isaksson², M., Joensen³, H.P., Lahtinen⁴, J. Logemann⁵, K., Pálsson⁶, S. E., Roos⁷, P., Suolanen⁸, V.

¹ Norwegian Radiation Protection Authority, Norway
² University of Gothenburg, Sweden
³ Fróðskaparsetur Føroya, Faroe Islands
⁴ Radiation and Nuclear Safety Authority, Finland
⁵ University of Iceland, Iceland
⁶ Geislavarnir Rikisins, Iceland
⁷ Risø DTU, Denmark
⁸ Technical Research Centre of Finland, Finland

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Abstract

In the report, consequences of hypothetical severe nuclear accidents releases to Nordic marine environment are preliminary considered. The considered marine area comprises the Baltic Sea (Sweden, Denmark, Finland) and the North Atlantic (Iceland, Faroes, Norway) areas. The hypothetical severe nuclear accidents can be related to nuclear power plants, nuclear powered submarines or ice-breakers.

Quite comprehensive survey on radioactive source terms of extremely severe nuclear power and submarine accidents has been done. This enables to estimate more realistically possible radioactive releases of various elements and nuclides to marine environment. One recent reference is of course the Fukushima accident and estimated releases there.

The marine flows and dilution circumstances around the Nordic nuclear power plants and in the Baltic Sea area in general, has been studied. Respectively marine flows related to Iceland and Faroes coasts are considered with measured data and with preliminary 3D-model simulations. The substantial depth of sea water in the North Atlantic affect vertical concentration profiles to some extent. At Icelandic or Faroese waters, a potential submarine accident would likely occur in a well defined water mass, and radioactivity from the accident would be detected and spread with the flow regime of the water mass in the world ocean.

Based on hypothetical severe accidents scenarios, preliminary consequence calculations has been done. It should be emphasised that the considered severe accident cases, considered in this study, do not directly attach any specific Nordic nuclear power plant or any specific submarine type. The considered radioactive releases will, however, provide specified references for more extensive consideration of environmental consequences of severe - or minor – radioactive releases to Nordic marine environment.

As a reference, the release amounts from a 3000 MWth reactor size were used. Based on source term analyses, the chosen release fractions in the study were: iodine 20% (of the total core inventory), caesium 10%, tellurium 10%, strontium 0.5%, ruthenium 0.5%. The considered release event to marine environment were assumed to start ten hours after shutdown of the reactor. Total released amounts of the most important nuclides were estimated to be: \(4.85 \times 10^{17}\) Bq (I-131), \(7.29 \times 10^{16}\) Bq (Cs-134) and \(4.17 \times 10^{16}\) Bq (Cs-137).

Due to the highly contaminated sea food, the arising doses to human from a hypothetical severe nuclear power plant accident would be high especially in local sea area. Based on preliminary results, annual individual doses could be ten to some hundreds of millisieverts from local sea area. The most important nuclides were Cs-134, Cs-137 and I-131 causing 96% of the total ingestion dose.

In the Baltic Sea area, the arising doses from a severe nuclear power plant accident assumed to happen e.g. at Gulf of Finland, would be about 1/10000 compared to doses in the local sea area. Thus the arising maximum annual individual dose for fish pathway is in the level of 0.1 mSv in the Baltic Sea area.
Submarine accident assumed to happen at Icelandic waters, has been analysed in the study. The calculated collective dose rates to man as well as doses to a critical group are significantly lower than doses from natural sources. However, in local considerations dose-rates are significantly higher than the negligible component to the annual individual dose obtained from natural sources (UNSCEAR, 2000) and, therefore, have to be taken into consideration during evaluation of the accident consequences.

Key words

severe radioactive releases, marine environment, nuclear power plants, submarines, doses
COSEMA

COnsequences of SEvere radioactive releases to Nordic MArine environment

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Contributors:

Mikhail Iosjpe, Norwegian Radiation Protection Authority, Norway
Mats Isaksson, University of Gothenburg, Sweden
Hans Pauli Joensen, Fróðskaparsetur Fôroya, Faroe Islands
Juhani Lahtinen, Radiation and Nuclear Safety Authority, Finland
Kai Logemann, University of Iceland, Iceland
Sigurður Emil Pálsson, Geislavarnir Rikisins, Iceland
Per Roos, Risø DTU, Denmark
Vesa Suolanen, Technical Research Centre of Finland, Finland

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1 Introduction

In the activity marine input data and preliminary consequences of hypothetical severe nuclear accidents releases to Nordic marine environment are considered. The considered marine area comprises the Baltic Sea (Sweden, Denmark, Finland) and the North Atlantic (Iceland, Faroe Islands, Norway) areas. The hypothetical severe nuclear accidents can be related to nuclear power plants (NPP), nuclear powered submarines or ice-breakers.

Quite comprehensive survey on radioactive source terms of extremely severe nuclear power and submarine accidents has been done. This enables to estimate more realistically possible radioactive releases of various elements and nuclides to marine environment. One recent reference is of course the Fukushima accident and estimated releases there.

The marine flows and dilution circumstances around the Nordic nuclear power plants and in the Baltic Sea area in general, has been studied. Respectively marine flows related to Iceland and Faroes coasts are considered with measured data and with preliminary 3D-model simulations. The substantial depth of sea water in the North Atlantic affects vertical concentration profiles to some extent.

The element specific marine transfer data, like sorption factors, has been reviewed. The sorption characteristics of various elements affect their behaviour and distribution between water and suspended solids in sea. Further this sorption factor creates the concentration distributions between sea water and bottom sediment.

Based on hypothetical severe accidents scenarios, preliminary consequence calculations have been done. It should be emphasised that the considered severe accident cases, considered in this study, do not directly attach any specific Nordic nuclear power plant or any specific submarine type. The considered radioactive releases will, however, provide specified references for more extensive consideration of environmental consequences of severe - or minor – radioactive releases to Nordic marine environment.

This report is an interim report of the planned two years research activity.
2 Hypothetical severe nuclear accidents in Nordic marine environment

Around the Baltic Sea there are several nuclear power plant units also in Sweden and in Finland. In Forsmark there are three BWR’s (2x2928 MW\textsubscript{th} and one 3300 MW\textsubscript{th}). In Ringhals there are four reactors: one BWR (2540 MW\textsubscript{th}) and three PWR’s (2652, 3135 and 2775 MW\textsubscript{th}). In Oskarshamn there are three BWR’s: 1375 MW\textsubscript{th}, 1800 MW\textsubscript{th} and 3300 MW\textsubscript{th}. In Loviisa there are two PWR’s (2x1500 MW\textsubscript{th}) (Lahtinen, J., 2012). A summary of nuclear facilities around the Baltic Sea is presented e.g. in an earlier study (Nielsen, S.P., et al., 2010).

In can be concluded that the greatest thermal reactor power of 3300 MW (corresponds to about 1000 MW\textsubscript{e}) represent the highest level of radionuclide inventories which could partially be released from the core in a hypothetical severe accident. This kind of reference accident case, so called worst case accident scenario, does not refer to any specific reactor in Nordic countries, but provides a picture of highest environmental consequences which could appear with very low probability. Consequences of smaller radioactive releases to Nordic marine environment can then quite easily be estimated based on the worst case accident results. Severe nuclear power plant accidents releases and consequences are planned to be considered starting from locations of current nuclear power plants in Finland and Sweden.

A severe nuclear power plant or submarine accident could result e.g. from operational reasons, coolant leakages (LOCA-accidents) or external treats. The radioactive source term from a severe damaged reactor core is in the study mainly assumed to be consisted of soluble substances like caesium and iodine radionuclides. The source term evaluation will be based on an assumption that functioning of all cooling safety systems of the considered reactor has been lost. In this case the reactor core is expected to melt finally significantly, causing large releases of volatile nuclides to the marine environment. The effect of duration of the source term will also be considered, because it is expected that a shorter release will produce elevated seawater and sediment concentrations at the local sea area, near the considered nuclear power plant or a submarine vessel. The released radionuclides will further disperse via marine flows to the whole Baltic Sea area or to the North Atlantic. Despite large dilution, the released radionuclides will cause some collective exposure also in the whole Baltic and North Sea areas.

Nuclear-powered submarine accidents near Iceland or the Faroese coasts might create special threats for the local marine ecology. These untypical radioactive release events in Atlantic are considered in consequence assessments of the activity as well.

References


3 Marine flows

3.1 Baltic Sea area

M. Isaksson, P. Roos, V. Suolanen

Marine flows around the Forsmark NPP and Ringhals NPP

Modelling of the water movements and ecological impact has been performed for the estuarine area outside the Forsmark power plant. Model estimations by Engqvist & Andrejev (1999) of the water exchange of the area adjacent to the plant as well as for the whole Baltic showed good resemblance with observed circulation.

Kumblad et al. (2006) was able to estimate the concentration of radionuclides in a modelled ecosystem with bioconcentration factors for plants and adsorption coefficients (K_d) as input parameters. The model was based on site-specific carbon dynamics and three radionuclide specific mechanisms: plant uptake, excretion by animals, and adsorption organic surfaces. The model suggest that the water exchange rate in the area is important considering radionuclide exposure to organisms, due to dilution of the water as well as by replacing the plankton with organisms that are not contaminated.

Concerning the vicinity of the Ringhals NPP, Holtegaard Nielsen (2005) presents data for the circulation I the Kattegat. In contrast to the common description that a large part of the area is governed by a basic estuarine circulation, Nielsen found anti-cyclonic circulation in a large part of the upper layer. This circulation was driven by a density gradient at the border between Kattegat and Skagerrak.

Spokes et al. (2006) found that the coastline and the islands within the Kattegat influence the entire Kattegat Sea region. The influence of the land masses gives rise to horizontal gradients in a large number of parameters. Atmospheric transport and deposition must therefore, according to Spokes et al., be modelled using the individual atmospheric conditions.

Marine flows around the Loviisa NPP

Generally, in the Gulf of Finland there is a circulation flow counter-clockwise, following the coasts of Estonia, Russia and Finland (Adrejev, et al., 2004). Thus the salinity of the water is slightly lower at the coastal area of Finland than in the coast of Estonia.

The islands restrict to some extent sea water flow from the Loviisa NPP local sea area Hästholmsfjärden to elsewhere of the Gulf of Finland. About distance of five kilometres from the plant, the areal density of islands decreases and the average depth of the sea is about 30 - 40 meters.

The water exchange rate of the local sea area beside the plant is 57 m³/s in normal operational use mode. Without cooling flow rate of the plant, natural water exchange rate in local sea area is about 28 m³/s. The corresponding water turnover of the local sea is about eight times per year. So the cooling flow rate determines the water exchange rate in normal operational use of the plant.
In this study it is however conservatively assumed that the cooling system is damaged during the release and dispersion phases of radionuclides in a severe nuclear power plant accident event. The effective dilution in local sea area is smaller in the case of natural flow circumstances in the local sea area.

References


3.2 Faroes

H. P. Joensen

A brief overview of ocean currents and radioactivity around the Faroe Islands is given in this section.

Main currents

Figure 1 gives an overview of the main surface current systems in the North Atlantic and the Nordic Seas (AMAP, 2010; Aure, J. et. al., 1998).

![Figure 1. Overview of main currents in the North Atlantic area (AMAP, 2010; Aure et. al., 1998)](image)

The main currents in the upper layer closer to the Faroe Islands and Iceland are illustrated in Figure 2 (Hansen, 2000). Warm North Atlantic Water (NAS, IS) is flowing northward with branches around the Faroe Islands and Iceland into the Norwegian Sea in the north, where it is cooled down and partly sinks to deeper layers. The main water flux into the Norwegian Sea is between Iceland and Scotland. A slope current is northward along the Scottish and the Norwegian shelf. Cold water (the East Greenland Current, EGS) flows from north southward along East Greenland through the Denmark Strait in the south, and continues westward south of Greenland. A northern branch flows eastward north of Iceland and towards the Faroe Islands (the East Icelandic Current, EIS), where it meets warm Atlantic Water. The Icelandic Front (IF) is found where the
warm Atlantic Water from the south meets colder water from the north. The front separates the two water masses. It is relatively close to the Faroe Islands, and the warm Atlantic Water flow north of the Faroes (the Faroe Current, FS) becomes a narrow eastward flow.

The main pattern of the southward overflow at lower depth from the north across the Greenland-Scotland ridge and into the North Atlantic is shown in Figure 3 and 4. It contains cold water from the deep layers in the north. In the Faroese area, the main overflow occurs in the bottom layer of the Faroe-Shetland channel in the east, between Shetland and the Faroe Islands. The overflow is part of the mass balance system between northward and southward water flow that again is part of the great conveyor belt known in oceanography, i.e. the thermohaline circulation in the world ocean (Fig. 5).

Water masses and radioactivity

Ocean water is characterized by physical and chemical properties as density, temperature and salinity. The world ocean contains large water bodies that can be identified according to their physical and chemical properties. The water bodies are known as “water masses” in oceanography.

Figure 6 illustrate the average water mass distribution around the Faroe Islands. The boundaries between the masses will always be somewhat ambiguous. They have different origins, according to the flow patterns in the open ocean, and this needs to be considered in the case of e.g. a submarine accident. A potential submarine accident would likely occur in a well defined water mass, and radioactivity from the accident would be detected and spread with the flow regime of the water mass in the world ocean.

Vertical profiles of Cs-137 and Sr-90 have been taken around the Faroe Islands. Results from a survey in August 1990 at a station north of the islands (Fig. 7) are shown in Figure 8, together with the ratio between the activity concentrations (Dahlgaard et al., 1991). The position is at 63°N20°N6°05’W, where the bottom depth is 2400m. The origin of the samples as related to water mass specification was determined from hydrographical analyses. A notable maximum is observed in the profiles at 400m. The ratios indicate input of the isotopes from other sources than global fallout. The range of the isotope ratio is 2.1-3.0, and Dahlgaard et al. conclude that it corresponds to increased input from Sellafield/Chernobyl, and that the peak at 400m depth as based on results from their hydrographical measurements corresponds to input of seawater from the Greenland Sea (cf. Fig.4). The lowest ratio of 2.1 at 1000m may still be considered relatively high compared to the fallout ratio of about 1.5, as this water had not recently been in contact with the atmosphere.

Long term time series of radioactivity in Faroese waters are shown in Figures 9 and 10 (AMAP, 2010), together with measurements from off the west and east coasts of Greenland. The activity concentrations are generally observed to be lower off the Faroe Islands than off the Greenland coasts. A signal from the Chernobyl accident can be seen in the Faroese data set.
Fig. 2. Upper layer water flows. (Hansen, 2000).

Fig. 3. Main pattern of overflow water. (Hansen, 2000).
Fig. 4. Cold southward flow over the Greenland-Iceland-Scotland ridge. The blue area illustrates the depth below 1000m (Hansen, 2000).

Fig. 5. The conveyor belt showing the thermohaline circulation in the world ocean (picture from internet).
Fig. 6. Usual water mass distribution. (Hansen, 2000).

Fig. 7. Bottom topography. Depth profiles were taken at the station marked with the red dot.
Fig. 8. Profiles of Cs-137 and Sr-90 north of the Faroes in August 1990 (cf. Fig. 6).

Fig. 9. Cs-137 in seawater off the coasts of the Faroe Islands and Greenland.
Fig. 10. Sr-90 in seawater off the coasts of the Faroe Islands and Greenland.

References


3.3 Iceland

S. E. Pálsson

The following are excerpts from the MARICE-E-report MER-13-2012, which give a glimpse of the structure of the marine model used at the University of Iceland and which will be used for further work within COSEMA.

Introduction

In order to simulate the hydrography of Icelandic waters the workgroup MARICE at the University of Iceland has developed the numerical ocean model CODE. With this report a detailed description of the recent model version CODE 9.221 is given and its output is presented: the hydrography of Icelandic waters during the time period 1992 to 2006. The model was forced by the 6 hourly NCEP/NCAR re-analysis atmospheric fields. Daily river discharge data of 58 Icelandic rivers, estimated by the hydrological model WaSiM operated by the Icelandic Meteorological Office, were included as well as all available CTD profiles recorded from 1992 to 2006 in Icelandic waters. The CTD data was assimilated into the simulation. I.e. with an iterative procedure correction terms were determined which minimised the deviation between simulated and observed temperature and salinity profiles.

The presentation of the model output is confined to charts of monthly mean flow, temperature and salinity at the depth of 50 m and to overall model error estimations. For a more profound analysis of the data set the reader is referred to the following publications of the authors.

Model description

CODE (Cartesian coordinates Ocean model with three-Dimensional adaptive mesh adaption and primitive Equations) is a three-dimensional, primitive equations, z-level, coupled seaice/ocean model. The basic idea behind CODE is the simulation of basin-scale ocean dynamics (length scale in the order of 10000 km) including the small-scale structures, with length scales less than 10 km, of selected areas of interest. Additionally the computational costs of the simulation should be minimised to enable the computation of multi-decadal runs within an acceptable length of time. Both points could be realised using the technique of adaptive mesh refinement. Though this involves more complicated numerical methods the disadvantages of conventional nesting (higher computational effort, missing coupling between several model runs, numerical errors at open boundaries) or finite element (higher computational effort) approaches could be avoided. The simulation presented here – entire North Atlantic/Arctic Ocean with highly resolved (1 km) Icelandic waters – was computed on an Intel Xeon 3.33 GHz CPU and needed 92 hours for the simulation of one year.

First CODE application in COSEMA

Based on topographic and hydrographic criteria nine compartment boxes, horizontally dividing the Icelandic waters, were defined (Fig. 17 and Table 1). These definitions were transferred into the ocean model and a series of model experiments were carried out. Within these experiments the mean current and diffusion fields averaged over the
period 1992 to 2006 were used. At the beginning of each model run a mathematical tracer concentration was set to 1 within one of the boxes. Then the advective and diffusive spreading of this concentration was simulated. After the simulation time of 24 hours the model was stopped, and the according flux rates between the boxes were computed (Fig. 18).

Fig. 11. Schematic process of adaptive grid refinement, following the algorithm of Khokhlov (1998). The large cube on the left side (adaptation level 0) is split into 8 “children” of adaption level 1. Hence the model equations are no longer solved on the “parent cell”. However, the “parent cell” is not removed from the computer’s memory. It is obtaining the average properties of its children at each time step instead.

Overall view of model over the North Atlantic:
Fig. 12. The computational mesh after the first step of horizontal mesh refinement.

Fig. 13. The computational mesh after the fourth step of horizontal mesh refinement.
Fig. 14. The computational mesh after the final seventh step of horizontal mesh refinement.

Fig. 15. The computational mesh’s vertical structure.
Fig. 16. The location and mean discharge of rivers included within the simulation.
Fig. 17. Definition of compartmental boxes for COSEMA modelling.

Table 1. Volume and depth of boxes.

<table>
<thead>
<tr>
<th>box no.</th>
<th>volume (m³)</th>
<th>mean depth (m)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>0.30875736E+14</td>
<td>0.41388681E+03</td>
</tr>
<tr>
<td>2</td>
<td>0.45874487E+13</td>
<td>0.19979407E+03</td>
</tr>
<tr>
<td>3</td>
<td>0.14862981E+14</td>
<td>0.39440656E+03</td>
</tr>
<tr>
<td>4</td>
<td>0.42704377E+14</td>
<td>0.69592224E+03</td>
</tr>
<tr>
<td>5</td>
<td>0.50321238E+14</td>
<td>0.6282296E+03</td>
</tr>
<tr>
<td>6</td>
<td>0.11065060E+15</td>
<td>0.92798999E+03</td>
</tr>
<tr>
<td>7</td>
<td>0.69452649E+14</td>
<td>0.10830667E+04</td>
</tr>
<tr>
<td>8</td>
<td>0.40931894E+14</td>
<td>0.41316107E+03</td>
</tr>
<tr>
<td>9</td>
<td>0.51804176E+14</td>
<td>0.84404614E+03</td>
</tr>
</tbody>
</table>
Fig. 18. Boxes with transfer parameters, flow rates between boxes in Sverdrup (1 Sv = $10^6$ m$^3$ m$^{-1}$).

References


4 Radioactive source term analyses

4.1 NPP accident source term

J. Lahtinen

4.1.1 Background

At the project meeting in March it was decided that the releases to the ocean in Fukushima should be used as a basis of the COSEMA source term. It is known that the situation in Fukushima was quite a complex one: there were three reactor facilities affected and there were planned and unplanned releases. In addition, deposition of airborne radioactive releases onto sea also constituted a source that – according to some estimates – is about the same order or even bigger as the direct releases to the ocean. Rain water washout of contaminated soils has also been mentioned but this contribution will become detectable in course of time as the concentrations along the coast have decreased.

Several papers and other documents addressing the marine source term of Fukushima have been published (see the list of references). Some assessments rely mostly on measurements of concentrations in sea water, some on measurements and model calculations, and a few primarily on calculations. Most documents deal only with caesium (\(^{137}\text{Cs}, \^{134}\text{Cs}\)) and (sometimes) \(^{131}\text{I}\). Estimated quantitative values of direct releases to the ocean vary, although it is generally agreed that the planned release of waste water which was "slightly contaminated" is insignificant as compared to the unplanned releases:

- \(^{137}\text{Cs}: \) from 3.5 to 27 PBq.
- \(^{134}\text{Cs}: \) about the same as for \(^{137}\text{Cs}\).
- \(^{131}\text{I}: \) from 11 to about 80 PBq.

Better and more reliable estimates are likely to be available after the UNSCEAR report will be published (Weiss, 2012).

STUK, which was responsible for defining the NPP source term to be used in COSEMA calculations, decided to use the paper of Bailly du Bois et al. (2011) as the basic source for source term estimation. It is likely that the source term – described originally in the project document "Marine source term of Fukushima NPP accident for NKS/COSEMA project" (Lahtinen; STUK, rev. 2 9.5.2012) – is conservative; this was discussed briefly at the project meeting in Oslo in September but no changes were made.

One of the reasons to use the paper of Bailly du Bois as a corner stone was that it is based on measurements and that it considers also some other nuclides than caesium isotopes and \(^{131}\text{I}\).

4.1.2 Fukushima source term

Bailly du Bois et al. (2011) took the advantage of measurement results when estimating the marine source term of Fukushima (Fig. 19). They derive the following conclusions:
Fig. 19. Evolution of $^{137}\text{Cs}$ concentrations and $^{131}\text{I}/^{137}\text{Cs}$ ratios in sea water at less than 2 km from the Fukushima Dai-ichi power plant (Bailly du Bois et al., 2011).

- Release of 27 PBq (12 PBq – 41 PBq) of $^{137}\text{Cs}$ from March 21 to July 18.
- $^{134}\text{Cs}/^{137}\text{Cs}$ concentration ratio was close to 1 and the decay-corrected $^{131}\text{I}/^{137}\text{Cs}$ ratio close to the plant was 24–18 from March 26 to April 8.
- $^{90}\text{Sr}/^{137}\text{Cs}$ and $^{99}\text{Tc}/^{137}\text{Cs}$ concentration ratios were 0.02 and 0.01 respectively (rough estimates).

In order to define a source term based on Bailly du Bois et al. one can make the following assumptions:

- In Fukushima all contaminated water was released from the core of Unit 2 (BWR type, 760 MW, 2380 MWth). (This of course is not true.)
- The release took place from March 26 to April 8.
- $^{134}\text{Cs}$ and $^{137}\text{Cs}$ activity concentrations in sea water were the same.
- Decay-corrected $^{131}\text{I}/^{137}\text{Cs}$ concentration ratio in water was 20.
- $^{90}\text{Sr}/^{137}\text{Cs}$ and $^{99}\text{Tc}/^{137}\text{Cs}$ concentration ratios in water were 0.02 and 0.01 respectively.
- Total $^{137}\text{Cs}$ release was 25 PBq.

From the above the released (decay-corrected for I-131) total activities can be estimated:
- $^{137}\text{Cs}$: 25 PBq (corresponds approximately to a release fraction of 11 %)\(^1\).
- $^{134}\text{Cs}$: 25 PBq (11 %)\(^1\)
- $^{131}\text{I}$: 500 PBq (23 %)\(^1\)
- $^{90}\text{Sr}$: 0.5 PBq (0.3 %)\(^1\)
- $^{99}\text{Tc}$: 0.25 PBq ($^{99}\text{Tc}$ activity originates apart from direct fission also from the decay of $^{99}\text{Mo}$ and $^{99m}\text{Tc}$-99)\(^2\)

If one follows here the same conventional procedure as in the case of releases to the atmosphere, the caesium release fraction given above can be applied to the caesium group (see Table 2), $^{131}\text{I}$ release fraction to the iodine group and $^{90}\text{Sr}$ release fraction to the strontium group. $^{99}\text{Tc}$ implies that nuclides in the ruthenium group were also released. This is supported by the fact that $^{58}\text{Co}$ was detected in the water too (TEPCO, 2011). In addition, tellurium (and $^{132}\text{I}$) was found (IRSN, 2011a; IRSN, 2011c).

Table 2. Nuclide groups (NUREG, 1990)\(^3\).

<table>
<thead>
<tr>
<th>Inert gases</th>
<th>Kr-85, Kr-85m, Kr-87, Kr-88, Xe-133, Xe-135</th>
</tr>
</thead>
<tbody>
<tr>
<td>Iodine</td>
<td>I-131, I-132, I-133, I-134, I-135</td>
</tr>
<tr>
<td>Cesium</td>
<td>Rb-86, Cs-134, Cs-136, Cs-137</td>
</tr>
<tr>
<td>Tellurium</td>
<td>Te-127, Te-127m, Te-129, Te-129m, Te-131m, Te-132, Sb-127, Sb-129</td>
</tr>
<tr>
<td>Strontium</td>
<td>Sr-89, Sr-90, Sr-91, Sr-92</td>
</tr>
<tr>
<td>Ruthenium</td>
<td>Co-58, Co-60, Mo-99, Tc-99m, Ru-103, Ru-105, Ru-106, Rh-105</td>
</tr>
<tr>
<td>Lanthanum</td>
<td>Y-90, Y-91, Y-92, Y-93, Zr-95, Zr-97, Nb-95, La-140, La-141, La-142, Pr-143, Nd-147, Am-241, Cm-242, Cm-144</td>
</tr>
<tr>
<td>Cerium</td>
<td>Ce-141, Ce-143, Ce-144, Np-239, Pu-238, Pu-239, Pu-240, Pu-241</td>
</tr>
<tr>
<td>Barium</td>
<td>Ba-139, Ba-140</td>
</tr>
</tbody>
</table>

\(^1\) The nominal equilibrium inventory of the Olkiluoto BWR (2500 MW\(\text{th}\)) is used as a reference. Note that the actual Fukushima inventory depends on the fuel burn-up and the power history before scram (and also partly on the fuel composition details).

\(^2\) $^{99}\text{Tc}$ activities are normally not given in the lists of important radionuclides in a reactor.

\(^3\) There also exist groupings that differ a bit from the one presented here.
4.1.3 COSEMA source term

The nuclear power plant sites in COSEMA are Loviisa (PWR, 1500 MW\(_{th}\)), Forsmark (BWR, 3300 MW\(_{th}\)), Ringhals (PWR, 3135 MW\(_{th}\)) and Oskarshamn (BWR, 3300 MW\(_{th}\)). There are several units at every site but those mentioned have the greatest thermal power. If actual inventories are not available, the inventories of the Loviisa and Olkiluoto reactors can be scaled and used in calculations.

As a very crude approximation one may assume that the release fraction for the tellurium group is the same as that for caesium and the release fraction for the ruthenium group is the same as that for strontium. Taking this and the reasoning in the preceding section into account the release fractions for the COSEMA studies are chosen to be: iodine 20 %, caesium 10 %, tellurium 10 %, strontium 0.5 %, ruthenium 0.5 %.

Other groups with smaller release fractions can be considered if needed.

It is realistic to assume that there is a delay between the reactor shutdown and start of the release. A 10-hour delay could be used, for example.

Two release periods are to be considered: three days and three weeks.

References


In addition, a special issue of the Journal of Environmental Radioactivity (volume 111, September 2012) *Environmental Impacts of the Fukushima Accident (Part I)* contains some papers dealing with releases to the sea.
4.2 Submarine accident source term

M. Iosjpe

Inventory

The source term consists of an inventory of radionuclides, released as a function of time and a release point. Each of these elements will be described below.

The core inventory has primarily two components: the fuel matrix itself and the fuel burn-up. While the fuel matrix itself has only indirect influence on the amount of fission products, the amount of transuranics and release rates will depend directly on the type of matrix. In the current work, with its emphasis on a credible approach, the most probable representation of a Russian third-generation submarine core is a core load with 63% enriched fuel with 259.7 kg U-235 in a dispersion (UO$_2$-Al/ UO$_2$-Zr) or intermetallic configuration (UA$_x$-Al) (Reistad, 2008). This composition has been verified to fit the only suggested core geometry for other than first-generation Russian submarines. However, as there exist an indefinite number of core configurations corresponding to various fuel volumes, the selection criterion has been to apply similar fuel density (4.5 Ug/cm$^3$) as that reported for Russian floating nuclear power plants under construction (Chuen and Reistad, 2007). A maximum credible inventory has been developed on the basis of a conservative approach to the average annual burn-up for third-generation reactors.

Average annual burn-up has been calculated to 30 effective full-power days (EFPD) and the maximum operational period hypothetically set to 20 years. At present, the average life-span for this class of vessels is 13.2 years. As the current decommissioning rate is higher than the commissioning rate, we may assume that this value will decrease slowly in the future. However, as the selection criterion has been a maximum credible burn-up, and normal vessel life is more than 13.2 years, we may assume 20 years of operation as a conservative estimate as a basis for calculating the radionuclide inventory at the time of the accident. The resultant burn-up is 114,000 MWD, or 269,000 MWD/tons of heavy metal. We have also assumed an operating power fraction of 0.5 at the time of accident, resulting in a high inventory of short-lived isotopes when the hypothetical accident occurs. The core inventory and core decay heat were developed using HELIOS 1.8 and SNF 1.2. HELIOS is a detailed reactor physics transport and burn-up code developed and supported by Studsvik Scandpower (Reistad, 2008).

Accident scenario

The hypothetical scenario forming the basis for this study, is if a core-melt / loss-of coolant accident (LOCA) (Reistad, 2008) was to occur together with another type of incident, such as an explosion. Then there would be a credible risk of substantial damage to all parts of the submarine. An explosion that ruptured the hull and provided water intrusion in the reactor compartment would also contribute to cooling the corium.

In this study, we will use the scenario described in Table 3, which corresponds to Scenario 1 from (Reistad, 2008).
Table 3. Release fractions for maximum credible accident for third-generation submarine.

<table>
<thead>
<tr>
<th></th>
<th>Phase 1: From t=0.1 days to t=1 year</th>
<th>Phase 2: From t=1 year</th>
</tr>
</thead>
<tbody>
<tr>
<td>Coremelt release</td>
<td>Immediate release of release fraction as given in Table 4 (High flux reactor)</td>
<td></td>
</tr>
<tr>
<td>Fuel corrosion</td>
<td>Constant release of fuel corrosion products: corrosion rate: 0.01 % of fuel material annually</td>
<td></td>
</tr>
</tbody>
</table>

Release fractions

The main methodological problem here is the lack of relevant information on fuel materials, and secondly, on radionuclide behavior in fuel matrixes under extreme conditions (high temperature, saltwater intrusion etc.). However, a civilian nuclear system with potentially similar attributes to those of third-generation reactors – high power densities, high enrichment levels and moderate burn-up levels (50%) – is found in civilian research reactors. The hypothetical correspondence in fuel design and fuel properties has formed the basis for assessments of fuel consumption, as in (Reistad, 2008). Few civilian research facilities have been analyzed on the basis of probabilistic methods; deterministic accident analysis remains the most applied method for these facilities. The source term evaluation for research facilities displays differences similar to those shown in Table 4, describing the release fractions for three HEU (highly enriched uranium) – fueled research reactors.
Table 4. Release fractions in the case of core meltdown following a LOCA (Abou Yehia and Bars, 2005).

<table>
<thead>
<tr>
<th></th>
<th>HIFAR</th>
<th>High flux reactor</th>
<th>SAFARI</th>
</tr>
</thead>
<tbody>
<tr>
<td>Noble gases</td>
<td>1</td>
<td>1</td>
<td>1</td>
</tr>
<tr>
<td>I</td>
<td>0.3</td>
<td>0.8</td>
<td>1</td>
</tr>
<tr>
<td>Br</td>
<td></td>
<td>0.8</td>
<td></td>
</tr>
<tr>
<td>Cs</td>
<td>0.3</td>
<td>0.8</td>
<td>0.163</td>
</tr>
<tr>
<td>Te</td>
<td>0.01</td>
<td>0.8</td>
<td>0.192</td>
</tr>
<tr>
<td>Rb</td>
<td>0.3</td>
<td>0.01</td>
<td></td>
</tr>
<tr>
<td>Ru</td>
<td>0.01</td>
<td>0.1</td>
<td>0.005</td>
</tr>
<tr>
<td>Ba, Rh, Sr</td>
<td></td>
<td>0.1</td>
<td></td>
</tr>
<tr>
<td>Actinides</td>
<td>0.01</td>
<td>0.1</td>
<td></td>
</tr>
<tr>
<td>Other</td>
<td></td>
<td>0.01</td>
<td></td>
</tr>
</tbody>
</table>

The second component of the release fraction is fuel degradation and corrosion. Based on the hypothesis of the fuel matrix and the accident scenario, the corrosion processes of the uranium-loaded fuel component, UO$_2$ or UAl$_x$, starts immediately when the seawater enters the primary circuit. Experiments for long-term dissolution of fuel elements in seawater obtained dissolution rates from 0.1 to 1% of the fuel per year at temperatures from 10 to 20°C (Petrov, 1991).

**Release Scenario**

The total and the individual releases of the radionuclides that had the most significant effect on the release rates during the initial and later phases of accidental releases are presented in Figure 20. As expected, the maximum release occurs during the initial period after the accident (the instant release fraction) with maximum values of $1.6 \times 10^{18}$ Bq at the beginning of release. Figure 20 shows that short-lived radionuclides of iodine and barium are most significant during the initial phase of release according to the present scenario, while $^{90}$Sr and $^{137}$Cs dominates in the final period of release.
Fig. 20. The release scenario for the initial time of 0-0.5 year (top) and for the time 0.5-100 years (bottom)
References


5 Calculation scenarios

NPP accident at coast of the Gulf of Finland

V. Suolanen

As an example of consequences of severe nuclear accidents in the Baltic Sea area, a hypothetical severe nuclear power plant accident taken place at the northern coast of the Gulf of Finland, was preliminary modelled in the study. A current nuclear power plant with two reactor units and the local sea area is shown in Fig. 21. below.

Fig. 21. Nuclear power plant and local sea area.

The radioactive source term to sea water was determined from the core inventory of the VVER-1000 reactor (Anttila, 2005) and applying further the element specific release fractions obtained in the source term analyses of this study (chapter 4.1, J. lahtinen). The used fuel burn-up was 50 MWd/kgU. Total released amounts of activity of the considered severe reactor accident is presented in Table 5.
Table 5. Total amounts of activity released to sea in a hypothetical severe VVER-1000 accident. There is 71 tU in the core of the reactor.

<table>
<thead>
<tr>
<th>Nuclide</th>
<th>Specific activity at shutdown (GBq/tU)</th>
<th>Core activity at shutdown (Bq)</th>
<th>Release fraction</th>
<th>Total release to sea (Bq), t&gt;10 h</th>
</tr>
</thead>
<tbody>
<tr>
<td>C-14</td>
<td>$5.00 \times 10^1$</td>
<td>$3.55 \times 10^{12}$</td>
<td>0.2</td>
<td>$7.10 \times 10^{11}$</td>
</tr>
<tr>
<td>Co-60</td>
<td>$2.45 \times 10^4$</td>
<td>$1.74 \times 10^{15}$</td>
<td>0.005</td>
<td>$8.70 \times 10^{12}$</td>
</tr>
<tr>
<td>Sr-90</td>
<td>$3.96 \times 10^6$</td>
<td>$2.81 \times 10^{17}$</td>
<td>0.005</td>
<td>$1.41 \times 10^{15}$</td>
</tr>
<tr>
<td>Tc-99</td>
<td>$7.12 \times 10^2$</td>
<td>$5.06 \times 10^{13}$</td>
<td>0.005</td>
<td>$2.53 \times 10^{11}$</td>
</tr>
<tr>
<td>I-131</td>
<td>$3.56 \times 10^7$</td>
<td>$2.52 \times 10^{18}$</td>
<td>0.2</td>
<td>$4.85 \times 10^{17}$</td>
</tr>
<tr>
<td>Cs-134</td>
<td>$1.03 \times 10^7$</td>
<td>$7.29 \times 10^{17}$</td>
<td>0.1</td>
<td>$7.29 \times 10^{16}$</td>
</tr>
<tr>
<td>Cs-137</td>
<td>$5.87 \times 10^6$</td>
<td>$4.17 \times 10^{17}$</td>
<td>0.1</td>
<td>$4.17 \times 10^{16}$</td>
</tr>
</tbody>
</table>

In order to study the effect of duration of the release to consequences, a short-term release of 3 days (Figures 22 and 23) and a long-term release of 21 days (Fig. 24) were considered. The highest activity release rate is for iodine (I-131) which can clearly be seen from the linear scale Fig. 22. Other important soluble release nuclides are C-134 and C-137.

In the long-term release assumption, the released total activity is dispersed for a longer time period. The effect of radioactive decay to the release rate of the short-lived I-131 can be seen from Fig. 24.
Fig. 22. Release rates temporal behaviour presented in linear scale for the most important radionuclides I-131, Cs-134 and Cs-137.

Fig. 23. Release rates of all important radionuclides in the short-term release assumption.
Fig 24. Release rates of important radionuclides in the long-term release assumption.
The aquatic transfer model consists of compartments for the local sea area close to nuclear power plant, the Gulf of Finland and the Baltic Sea dispersion area. Each water compartments has connection to bottom sediment layers (sedimentation term) and vice versa (resuspension term). Some main parameter values used in model calculations with Detra-code are presented in Table 6.

Table 6. Parameter values related to radionuclides transfer model of a hypothetical severe reactor accident at Gulf of Finland.

<table>
<thead>
<tr>
<th>Water comp. characteristics</th>
<th>Local sea area</th>
<th>Gulf of Finland</th>
<th>Baltic Sea</th>
</tr>
</thead>
<tbody>
<tr>
<td>volume (m$^3$)</td>
<td>1.0-10$^8$</td>
<td>5.5-10$^{11}$</td>
<td>1.4-10$^{13}$</td>
</tr>
<tr>
<td>water exchange rate (m$^3$/a)</td>
<td>8.8-10$^8$</td>
<td>6.0-10$^{11}$</td>
<td>5.0-10$^{12}$</td>
</tr>
<tr>
<td>suspended sediment load (kg$_s$/m$^3$)</td>
<td>5.0-10$^{-3}$</td>
<td>3.0-10$^{-3}$</td>
<td>4.0-10$^{-3}$</td>
</tr>
<tr>
<td>sedimentation rate (kg$_s$/m$^2$/a)</td>
<td>1.7-10$^{-1}$</td>
<td>1.7-10$^{-1}$</td>
<td>4.0-10$^{-1}$</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Sediment characteristics</th>
<th>surface sediment</th>
<th>buried sediment</th>
</tr>
</thead>
<tbody>
<tr>
<td>volume fraction of water</td>
<td>90%</td>
<td>72%</td>
</tr>
<tr>
<td>resuspension of sedimented material</td>
<td>10 % of total sedimentation</td>
<td></td>
</tr>
<tr>
<td>water exchange rate</td>
<td>1 a$^{-1}$</td>
<td></td>
</tr>
</tbody>
</table>

$K_d$-values (liter/kg$_s$) | $C_{fish}$ (Bq/kg$_s$)/(Bq/liter) ; (IAEA TRS 422 & 472)
| C             | 100 | 2000 |
| Co            | 5000| 1000 |
| Sr            | 10  | 2    |
| Tc            | 5000| 30   |
| I             | 100 | 10   |
| Cs            | 1000| 250  |

The activity concentrations obtained in the local sea area water after a severe accident are very high, which is illustrated in Fig. 25. The large dilution capacity of the Gulf of Finland and the Baltic Sea will effectively decrease the radionuclide concentrations in sea water.
Fig. 25. Maximum activity concentrations in sea water in local and areal scale after a severe reactor accident.

In case the highly contaminated sea food will be used by human, the arising doses would be high especially in local sea area (Fig. 26), total maximum annual individual dose about 600 mSv. Based on preliminary results the most important nuclides are Cs-134, Cs-137 and I-131 causing 96 % of the total ingestion dose.

Fig. 26. Dose estimates for fish consumption from local sea area at the Gulf of Finland after a hypothetical severe reactor accident.
In the consideration of the Baltic Sea area, radionuclides concentrations of dominant long-lived nuclides (Cs-134, Cs-137) are about 1/10000 compared to concentrations obtained in the local sea area, close to the damaged NPP. Thus the arising maximum annual individual dose for fish dose pathway in the Baltic Sea area is in the level of 0.1 mSv.

References

Anttila, M., Radioactive characteristics of the spent fuel of the finnish nuclear power plants, Posiva WR 2005-71.


IAEA TRS-472, Handbook of parameter values for the prediction of radionuclide transfer in terrestrial and freshwater environments, IAEA, Vienna, 194 p.
**Submarine accident at Iceland waters**

M. Iosjpe

**Brief description of the COSEMA compartment model**

The COSEMA model is based on the methodology developed for the NRPA box model, which uses a modified approach for compartmental modeling (Iosjpe et al., 2002). This methodology allows for simulation of radionuclide dispersion over time.

The compartments, which include the volumes, mean depth and water exchanges between boxes for the Iceland coastal waters, were developed during the COSEMA project by Geislavarnir Rikisins (Iceland). Additionally, two compartments surrounding the Iceland boxes were developed on the basis of the NRPA box model. The surface box structures for both models are shown in Figure 27.

![Fig. 27. The structure of the surface compartments in the COSEMA (top) and the NRPA (bottom) models and location of the potential accident (red dot).](image)

The COSEMA model adopts the sediment structure from the NRPA model, including the surface, mid-depth and deep sediment compartments for all water regions. Water-sediment interactions include sedimentation, diffusion of radioactivity through pore
water in sediments, resuspension, mixing due to bioturbation, particle mixing and a burial process for radionuclides in deep sediment layers. Radioactive decay is calculated for all compartments. The contamination of biota is further calculated from the known radionuclide concentrations in filtered seawater in the different water regions. Collective doses to the world population are calculated on the basis of seafood consumptions, in accordance with available data for seafood catches and assumptions about human diet in the respective areas (Nielsen et al., 1997; EC, 2000; IASAP, 2003).

The collective dose $D$ (manSv) can be determined using the following expression:

$$D = \sum_{j=1}^{m} DCF_j \sum_{l=1}^{k} \varphi_l \cdot CF_{lj} \sum_{i=1}^{n} A_{il} \int_{0}^{T} C_{ij}(t) \, dt,$$  

(1)

where $[0, T]$ is the time interval (y); $DCF_j$ (Sv/Bq) is the dose conversion factor for radionuclide $j (j = 1, 2, ..., m)$; $CF_{lj}$ (m$^3$/t) is the concentration factor for radionuclide $j$ in seafood of type $l (l = 1, 2, ..., k)$; $A_{il}$ (t/y) is catch of seafood of type $l$ in the model compartment $i (i = 1, 2, ..., n)$; $C_{ij}$ (Bq/m$^3$) is the concentration of radionuclide $j$ in filtered seawater in model compartment $i$; and $\varphi_l$ is the edible fraction for seafood of type $l$. The following assumptions (CEC, 1990; EC, 2000; IASAP, 2003) for the edible fractions of marine produce to the human diet have been used: 50 % for fish, 35 % for crustaceans and 15 % for molluscs).

Collective dose rates $DR$ can be defined using the following expression:

$$DR = \frac{D(t_2) - D(t_1)}{t_2 - t_1},$$  

(2)

where $D(t_1)$ and $D(t_2)$ are collective doses at times $t_1$ and $t_2$, respectively.

It is necessary to note that the model can also easily be used to provide information on impact doses/dose rates from different marine regions, and provide dose assessment to different population groups. Furthermore, the dose rate will be used in the present dose assessment because this parameter can easily indicate dose dynamic and is therefore widely used in recent investigations (EC, 2003; IASAP, 2003).

**Accident location**

The location (the compartment 2 in Figure 28) chosen for the accident was based on an evaluation of the radiological sensitivity of different marine areas. Radiological sensitivity analysis of Arctic marine regions shows that the shallow waters can be considered as the most vulnerable areas in the Arctic region, in terms of the effects of possible radioactive contamination (Iosjpe et al., 2003; Iosjpe, 2011; Iosjpe & Liland, 2012).
Results and discussion

The radioecological consequences of the potential scenarios leading to accidental releases of radioactivity have been evaluated on the basis of the calculated concentrations of radionuclides in typical sea foods, collective dose rates to man and individual doses for the critical groups and doses to marine organisms.

Concentration of radionuclides in seafood

The Food and Agriculture organisation of the United Nations and World Health Organisation have provided recommendations (guideline levels) for the maximum permissible concentration of radionuclides in foods, when contaminated after an accidental release of radionuclides (CAC, 2006). According to the Codex Alimentarius Commission (CAC, 2006) radionuclides can be separated into four groups. Examples of some typical radionuclides for each group are presented in Table 7.

Table 7. Examples of international guideline levels for radionuclides in food.

<table>
<thead>
<tr>
<th>Radionuclides in Foods</th>
<th>Guideline Level (Bq/kg)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Infant Foods</td>
</tr>
<tr>
<td>Group 1</td>
<td>$^{238}$Pu, $^{239}$Pu, $^{241}$Am</td>
</tr>
<tr>
<td>Group 2</td>
<td>$^{90}$Sr, $^{106}$Ru, $^{129}$I</td>
</tr>
<tr>
<td>Group 3</td>
<td>$^{60}$Co, $^{134}$Cs, $^{137}$Cs</td>
</tr>
<tr>
<td>Group 4</td>
<td>$^{3}$H, $^{14}$C, $^{99}$Tc</td>
</tr>
</tbody>
</table>

Following the CAC (2006) recommendations, the model calculations for fish, crustaceans and molluscs are provided separately for each group of radionuclides presented in Table 7.

It is clear that the highest level of sea food contamination is expected in box 2 (the accident location compartment). Results of the simulations of the radionuclide concentrations in seafood (fish, crustaceans and molluscs) for group 1 are shown in Figure 28. Results show the three most significant radionuclides in the group and the total concentration for the group.
Results of the model calculations indicate that the concentration of radionuclides from group 1 in seafood lies significantly under the CAC guideline levels for fish and crustaceans, but considerably exceeding the CAC guideline level for molluscs for infant food during the first four weeks after the accidental release began. The total concentration level of radionuclides in seafood for group 1 is heavily dominated by $^{238}$Pu. Therefore, it is interesting to note that the concentration of $^{238}$Pu in compartment 2 is one to three orders of magnitude higher than in other boxes (results are presented in Figure 29).
Fig. 29. Concentrations in sea waters in compartment 1-9.

Predicted concentration of Group 2 radionuclides in seafood is shown in Figure 30. The CAC guideline level is shown for comparison.

Fig. 30. Concentration of radionuclides (Group 2) in seafood.
The predicted concentration of radionuclides in fish is lower than the CAC guideline level for group 2 radionuclides. Results of the simulations for crustaceans and molluscs indicate that the radionuclide concentrations in the zone of the accident exceed the CAC guideline level for a period of approximately one to two months after the accident. The predicted maximum values of the radionuclide concentration in crustaceans and molluscs are around 120 and 700 Bq/kg, respectively. The radionuclides that impacted the concentration levels in seafood (for group 2) the most were $^{131}$I, $^{241}$Pu and $^{106}$Ru.

The concentrations of group 3 radionuclides in seafood are shown in Figure 31.

Fig. 31. Predicted concentration of radionuclides (Group 3) in seafood.

The results of the simulations for group 3 radionuclide concentrations in seafood indicate that the radionuclide concentrations in box 2 (the accident location) exceed the CAC guideline value of 1000 Bq/kg for a period of approximately one-two weeks after the accident. The concentration of radionuclides is dominated by the level of $^{132}$Te during these weeks. $^{126}$Sn and $^{144}$Ce (for molluscs) start to dominate the concentration level of group 3 radionuclides in seafood during the time following the two weeks after the accident.

Figure 32 shows that the contamination curves of seafood by group 4 radionuclides lies under the guideline levels for general food, but exceeds the guideline level for infant food for a period of approximately one week after the accident. $^{127}$Te, $^{129m}$Te dominate the radionuclide concentration during this initial time. During the time following this week,
$^{125}$Sb and $^{147}$Pm have a significant impact on the total concentration of radionuclides in fish, and $^{103}$Ru and $^{147}$Pm dominate the radionuclide concentrations in crustacean and molluscs.

Collective dose rates to man

The results presented in Figures 33 and 34 show that the maximum collective dose rates in the studied scenario, occur during the first year after the release of radioactivity. The maximum collective dose rate is approximately 58 manSv per year, with $^{134}$Cs, $^{137}$Cs and $^{126}$Sn having the highest impact on the maximum collective dose rate.
Fig. 33. Predicted collective dose-rates, manSv per year

Fig. 34. Impact of radionuclides to the collective dose rate (the first year after the hypothetical accident)

**Doses to the critical group**

In the present study we assume that the critical group is a population living on the coast of the sea region nearest to the accident location. The evaluation of the doses for this group will be based on an investigation of consumption patterns for the population living on the Norwegian coast and inland (Bergsten, 2003), where maximum seafood consumption is 200, 40 and 4 g/day for fish, crustaceans and molluscs, respectively.

The individual dose rates for the ingestion pathway have been calculated on the basis of expressions (1) and (2), where catchments of seafood were replaced by consumptions for the critical groups.

The proportions of the total calculated dose attributable to the different types of seafood are presented in Figure 35, corresponding to the maximum dose rate. Figure 35 shows that for the present scenario $^{134}$Cs, $^{137}$Cs and $^{126}$Sn were the three radionuclides that gave the most significant contribution to the doses received from ingestion of seafood for the critical group. It is also necessary to note that the impact of $^{144}$Ce is significant for the doses from crustaceans and molluscs.

The calculated maximum dose-rate equals 110 μSv yr$^{-1}$, which is significantly lower than the average annual dose of 1-10 mSv from nature sources. At the same time, this dose-
rate is significantly higher than range 1 - 10 $\mu$Sv yr$^{-1}$ for the negligible component to the annual individual dose from natural sources (UNSCEAR, 2000) and, therefore, has to be under consideration during evaluation of the accident consequences.

Fig. 35. Potential dose impact to the critical group from fish, crustaceans and molluscs
Conclusions of submarine accident analysis

The consequences of an accident with a modern Russian submarine were calculated on the basis of the most conservative scenario from the ones were under consideration in the present investigation.

Calculations indicate that, generally, concentration of radionuclides in seafood would be under the international guideline levels for different groups of radionuclides. Simultaneously, results of calculations indicated that concentrations of radionuclides for some marine organisms during initial time of release near the accident location exceeded guideline levels. Elevated levels of radionuclides in marine food products may lead to economical consequences in a market very sensitive to contaminants, even if they don’t exceed guideline levels.

Calculated collective dose rates to man as well as doses to a critical group are significantly lower than doses from natural sources, but at the same time, these dose-rates are significantly higher than the negligible component to the annual individual dose from natural sources (UNSCEAR, 2000) and, therefore, have to be taken into consideration during evaluation of the accident consequences.

References

Bergsten, C., 2005. Fish and Game Study, part B: “The consumption of foods that may be important when assessing the dietary intake of mercury, cadmium and PCB/dioxins, with a focus on population groups living on the coast and in the inland of Norway.” Oslo: Norwegian Food Safety Authority, 2005.


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6 Conclusions

In the study consequences of severe radioactive releases to Nordic marine environment has been preliminary considered. The research activity has covered areas of Nordic marine input data, radioactive source term evaluations for nuclear power plants and for submarine vessels, marine flows and dilution aspects, element specific sorption and transfer factors and preliminary radiation dose estimates to human.

As a reference, the release amounts from a 3000 MW_{th} reactor size were used. Based on source term analyses, the chosen release fractions in the study were: iodine 20\% (of the total core inventory), caesium 10\%, tellurium 10\%, strontium 0.5\%, ruthenium 0.5\%. The considered release event to marine environment were assumed to start ten hours after shutdown of the reactor. Total released amounts of the most important nuclides were estimated to be: $4.85 \times 10^{17}$ Bq (I-131), $7.29 \times 10^{16}$ Bq (Cs-134) and $4.17 \times 10^{16}$ Bq (Cs-137).

Due to the highly contaminated sea food, the arising doses to human would be high especially in local sea area. Based on preliminary results, annual individual doses could be ten to some hundreds of millisieverts from local sea area. The most important nuclides were Cs-134, Cs-137 and I-131 causing 96\% of the total ingestion dose.

In the Baltic Sea area, the arising doses from a severe nuclear power plant accident assumed to happen at Gulf of Finland, would be about 1/10000 compared to doses in the local sea area. Thus the arising maximum annual individual dose for fish pathway is in the level of 0.1 mSv in the Baltic Sea area.

Submarine accident assumed to happen at Icelandic waters, has been analysed in the study. The calculated collective dose rates to man as well as doses to a critical group are significantly lower than doses from natural sources. However, in local considerations dose-rates are significantly higher than the negligible component to the annual individual dose obtained from natural sources (UNSCEAR, 2000) and, therefore, have to be taken into consideration during evaluation of the accident consequences.

In the planned continuing phase of the activity, more detailed marine 3D flow simulations will be done and utilized for Icelandic and the Faroese waters. Additionally, important model validation against measured data is necessary to curry out e.g. for the Baltic Sea region.
In the report, consequences of hypothetical severe nuclear accidents releases to Nordic marine environment are preliminary considered. The considered marine area comprises the Baltic Sea (Sweden, Denmark, Finland) and the North Atlantic (Iceland, Faroes, Norway) areas. The hypothetical severe nuclear accidents can be related to nuclear power plants, nuclear powered submarines or ice-breakers.

Quite comprehensive survey on radioactive source terms of extremely severe nuclear power and submarine accidents has been done. This enables to estimate more realistically possible radioactive releases of various elements and nuclides to marine environment. One recent reference is of course the Fukushima accident and estimated releases there.

The marine flows and dilution circumstances around the Nordic nuclear power plants and in the Baltic Sea area in general, has been studied. Respectively marine flows related to Iceland and Faroes coasts are considered with measured data and with preliminary 3D-model simulations. The substantial depth of sea water in the North Atlantic affect vertical concentration profiles to some extent. At Icelandic or Faroese waters, a potential submarine accident would likely occur in a well defined water mass, and radioactivity from the accident would be detected and spread with the flow regime of the water mass in the world ocean.

Based on hypothetical severe accidents scenarios, preliminary consequence calculations has been done. It should be emphasised that the considered severe accident cases, considered in this study, do not directly attach any
specific Nordic nuclear power plant or any specific submarine type. The considered radioactive releases will, however, provide specified references for more extensive consideration of environmental consequences of severe or minor – radioactive releases to Nordic marine environment.

As a reference, the release amounts from a 3000 MW\textsubscript{th} reactor size were used. Based on source term analyses, the chosen release fractions in the study were: iodine 20% (of the total core inventory), caesium 10%, tellurium 10%, strontium 0.5%, ruthenium 0.5%. The considered release event to marine environment were assumed to start ten hours after shutdown of the reactor. Total released amounts of the most important nuclides were estimated to be: $4.85\cdot10^{17}$ Bq (I-131), $7.29\cdot10^{16}$ Bq (Cs-134) and $4.17\cdot10^{16}$ Bq (Cs-137).

Due to the highly contaminated sea food, the arising doses to human from a hypothetical severe nuclear power plant accident would be high especially in local sea area. Based on preliminary results, annual individual doses could be ten to some hundreds of millisieverts from local sea area. The most important nuclides were Cs-134, Cs-137 and I-131 causing 96% of the total ingestion dose.

In the Baltic Sea area, the arising doses from a severe nuclear power plant accident assumed to happen e.g. at Gulf of Finland, would be about 1/10000 compared to doses in the local sea area. Thus the arising maximum annual individual dose for fish pathway is in the level of 0.1 mSv in the Baltic Sea area.

Submarine accident assumed to happen at Icelandic waters, has been analysed in the study. The calculated collective dose rates to man as well as doses to a critical group are significantly lower than doses from natural sources. However, in local considerations dose-rates are significantly higher than the negligible component to the annual individual dose obtained from natural sources (UNSCEAR, 2000) and, therefore, have to be taken into consideration during evaluation of the accident consequences.

Key words severe radioactive releases, marine environment, nuclear power plants, submarines, doses