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Published in:
Proceedings of SPIE

Link to article, DOI:
10.1117/12.2289526

Publication date:
2018

Document Version
Publisher's PDF, also known as Version of record

Link back to DTU Orbit

Citation (APA):

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Low Temperature bonding of heterogeneous materials using Al$_2$O$_3$ as an intermediate layer

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ABSTRACT

Direct wafer bonding is a key enabling technology for many current and emerging photonic devices. Most prior work on direct wafer bonding has, however, focused on the Si platform for fabrication of silicon-on-insulator (SOI) and micro-electromechanical systems (MEMS). As a result, a universal bonding solution for heterogeneous material systems has not yet been developed. This has been a roadblock in the realization of novel devices which need the integration of new semiconductor platforms such as III-V on Si, Ge on Sapphire, LiNbO$_3$ on GaAs etc. The large thermal expansion coefficient mismatch in the hetero-material systems limits the annealing to low temperatures to avoid stressed films. This work explores the use of Al$_2$O$_3$ as an intermediate layer for bonding heterogeneous materials. The key to achieve a stronger bond is to maximize the hydroxyl group density of the bonding interfaces. The use of Al$_2$O$_3$ helps achieve that, since it has a high hydroxyl group density (around 18 OH/nm$^2$ at RT) which is approximately 4 times that of a Si surface. This work optimizes the bonding process using Al$_2$O$_3$ by studying the contribution of Al$_2$O$_3$ deposition parameters. An optimized process is presented and applied to bond GaAs on Sapphire and InP on SiO$_2$/Si.

Keywords: direct bonding, Al2O3, low temperature, Si photonics, integration, heterogeneous

1. INTRODUCTION

Often bonding of two different materials is needed to realize advanced devices, and then direct wafer bonding is a better and cleaner choice compared to polymer adhesive bonding, eutectic bonding, or anodic bonding etc. The requirements for a good direct bond are an ultra-clean and smooth hydrophilic surface. When bondable surfaces are brought in contact at room temperature, the two surfaces are initially bonded by hydrogen bonding. A high-temperature annealing process follows to achieve covalent bonds at the interface. The seminal work of Maszara et al.$^1$ and Tong and Gösele$^2$ still provide the fundamental understanding of direct wafer bonding. Maszara et al. highlighted the importance of high-temperature annealing for achieving high interface energy. Tong and Gösele, on the other hand, studied optimization of the annealing parameters to maximize the interface energy. This process technology, however, cannot be applied directly to heterogeneous material systems. First and most importantly, the difference in thermal expansion coefficient may limit the annealing temperature to avoid thermal stress in the bonded sample. InP wafers bonded to Si wafers, for example, start showing defects when annealed above 300 $^\circ$C.$^3$ Secondly, bonding is a surface phenomenon with a strong dependence on the surface chemistry of the bonding interfaces. Thus, the process technology developed for one set of wafers may or may not be adapted to a new pair of materials. Finally, most of the bonding process flows involve a surface activation step which may increase the surface roughness of the wafers. Often, it is recommended to break the surface bonds by an O$_2$ plasma or Ar sputtering followed by a dip in de-ionized water (DIW). A dip in water prior to bonding is often undesirable, especially when one of the wafers has micro-electro-mechanical structures (MEMS) defined.$^4$ This work aims to address all the above-mentioned concerns and suggests a low-temperature bonding process for hetero-material systems.

An ideal bonding method should be able to achieve a strong bond even with a low annealing temperature. The density of hydroxyl groups on the surface of the bonding wafers holds the key to a good bond. The higher
the number of hydroxyl groups, the higher is the number of linkages between the two wafers. A silicon surface has a hydroxy surface density of approximately 4 OH/nm$^2$ while an Al$_2$O$_3$ surface has a hydroxyl group density around 18 OH/nm$^2$. Thus, two wafers with Al$_2$O$_3$ as the bonding interface will be almost four times stronger than that of bare silicon. Furthermore, Al$_2$O$_3$ can be deposited with high precision using atomic layer deposition (ALD) at rather low temperature; thus it can be used as an intermediate layer also for bonding hetero-material systems. A high density of hydroxyl groups ensures a strong bond even at a low temperature. With limited studies in this direction, this work builds on the established knowledge and aims to establish a process flow which can be applied to most material systems.

2. EXPERIMENT

The Maszara blade test$^1$ is one of the most commonly used bond strength characterization methods. The Maszara test is relatively simple to carry out but is destructive. For III-V materials, however, the Maszara test is almost impossible to carry out, since the materials are too brittle for the test. Moreover, III-V materials are quite expensive to sacrifice for such characterization steps. Thus, in most cases, substrate etching is used as a qualitative method to characterize the bond quality of III-V materials. To address this concern, silicon wafers were used for understanding Al$_2$O$_3$ based bonding and optimizing the process technology. Later, the optimized process flow was applied to hetero-material systems and substrate etch was done to look at the bond quality qualitatively.

Figure 1 illustrates the basic process flow used in this experiment. Prime grade single crystal (100) 2-inch silicon wafers from a new wafer box were used for the experiments and no additional cleaning steps were done. Two silicon wafers were loaded into a commercial ALD chamber to deposit a few monolayers of Al$_2$O$_3$ and the wafers were pre-bonded right out of the chamber. By pre-bonding, we refer to the placement of bondable wafers together and the wafers being held by hydrogen bonds. The pre-bonded wafers were then placed in a commercial wafer bonding system for annealing at 300 °C for 60 min. A force of 2 kN was applied on 2-inch pre-bonded wafers during the annealing process to minimize voids from particles.

The interface energy of the bonded wafers was determined using the setup shown in Figure 2. The sample (bonded wafers with an inserted metal strip) was placed on a double side polished (DSP) 6-inch Si wafer. The sample was illuminated from below the Si wafer using an IR lamp and the image was collected using a camera from the top. A change in contrast between the bonded and de-bonded region was used to obtain the required parameters to calculate the interface energy. (Figure 3) A 50 μm steel strip was inserted between the bonded silicon wafers to cause delamination. The interface energy was calculated using

\[
\gamma = \frac{3}{32} \frac{Et^3y^2}{L^4},
\]

where $E$ is Young’s modulus of the material (Si), $t$ is the thickness of the wafers, $y$ is the thickness of the blade and $L$ is the crack length. An experimental error of ±15% is typically assumed for the Maszara test. At least four different measurements for each point were performed to obtain the standard deviation, shown in the results discussed next.
Clean wafers with surface roughness < 0.3 nm
2 nm ALD Al$_2$O$_3$ Deposition Pre-bond and Anneal

Figure 2. Schematic illustration of the setup used for the Maszara test. A bonded sample with an inserted metal strip is placed on a double side polished (DSP) 6" Si wafer. An IR lamp below the Si wafer is used to illuminate the sample. An IR camera with an adjustable lens is fixed on top of the setup for capturing an image of the sample.

Figure 3. IR camera image with overlayed information obtained from the Maszara test using the setup shown in Figure 2.

3. DISCUSSION

Bonding is a surface phenomenon which implies that the material properties of the surface should be important. The bonding process discussed here uses Al$_2$O$_3$ as the intermediate layer. Thus, the deposition parameters of Al$_2$O$_3$ influence the achieved interface energy. In particular, the effects of the thickness of ALD Al$_2$O$_3$ and the ALD temperature on the interface energy are explored in this paper.

To study the effect of ALD Al$_2$O$_3$ on the bond quality, different thicknesses of Al$_2$O$_3$ were deposited at 200 °C on Si wafers, which were then bonded and annealed at 300 °C for 60 min. Figure 4 shows the bond strength of bonded silicon wafers with different thicknesses of the intermediate layer. The thickness of ALD Al$_2$O$_3$ referred
Figure 4. Interface energy of bonded Si wafers using Al$_2$O$_3$ based bonding (measured using the Maszara test) plotted against the thickness of intermediate Al$_2$O$_3$ used. The bonded samples were annealed at 300 °C for 60 min using a commercial wafer bonding setup.

As expected, the thickness of the deposited Al$_2$O$_3$ did not have a significant influence on the interface energy of the bonded samples. As little as 2 nm of Al$_2$O$_3$ was enough to form a strong bond. The minimum deposited thickness of Al$_2$O$_3$ discussed in this paper is 2 nm to ensure a uniform film deposition of Al$_2$O$_3$ on the entire wafer. The interface energy corresponding to 50 nm of Al$_2$O$_3$ was slightly lower than that of the remaining samples. The achieved bond strength was quite high and there were no voids observable in the IR camera. Many reports suggest the need for a thick oxide film to achieve a void-free bonding.\textsuperscript{13–15} When a pre-bonded wafer is annealed, water molecules from the bond interface diffuse to the Si surface where they react with silicon to form silicon dioxide and hydrogen, the resulting hydrogen escapes to the interface to form voids. The hydrogen may also be dissolved in the thick oxide. However, Al$_2$O$_3$ is denser than SiO$_2$ and thus has a low diffusivity for water molecules.\textsuperscript{16} Low water diffusivity has also been shown by Ventonsa et al.\textsuperscript{17} using pre-annealed SiO$_2$. Thus, the water molecules most likely get trapped at the bond interface and fill up any nanovoids arising from surface roughness of the bonding wafers. The water molecules being denser than hydrogen occupy less volume and thus the voids are invisible.

The hydroxyl group density is important to maximize the interface energy. The hydroxyl group density is dependent on the material properties and temperature. Thus, the deposition temperature of ALD Al$_2$O$_3$ may also influence the interface energy. Figure 5 shows the bond energy measured for Si wafers bonded with 2 nm of ALD Al$_2$O$_3$ deposited at different temperatures. The wafers were then annealed at 300 °C for 60 min. No clear trend was observed; this may be partly due to the limited temperature region used for this study. Some wafers were also exposed to water vapour (humid environment) prior to pre-bonding. This ensured a saturated hydroxyl group density and this can be verified from the Figure 5. The interface energy of the bonded silicon wafers with a short water vapour exposure was independent of the ALD temperature. Ideally, the ALD coated wafers should be placed on a heat sink for a short time before bonding to ensure re-hydroxylation.

4. OPTIMIZED BONDING PROCESS

The wafers still need to be clean and have low surface roughness as is also necessary in direct bonding. However, there is no need for any surface preparation or activation. Deposition of ALD Al$_2$O$_3$ ensures a hydroxyl-rich surface without the need for any wet chemistry. More importantly, as little as 2 nm of Al$_2$O$_3$ is enough to
Figure 5. Interface energy of bonded Si wafers using Al$_2$O$_3$ based bonding (measured using the Maszara test) plotted for different ALD temperatures. The wafers were coated with approximately 2 nm of Al$_2$O$_3$. They were then pre-bonded with/without 30 sec of exposure to water vapor. The pre-bonded wafers were annealed at 300 °C for 60 min using a commercial wafer bonding setup before the Maszara test.

Figure 6. Interface energy of Si-Si wafer bonding as a function of the anneal temperature. Literature data due to Maszara et al.$^1$ and Tong and Gösele$^2$ are compared to our data from the optimized process using Al$_2$O$_3$.

Achieve a strong bond. The deposition temperature of Al$_2$O$_3$ is not very important, as long as the wafers are allowed to be re-hydrolyzed. The wafers should then be bonded and annealed at the maximum permissible temperature (considering the relative thermal expansion coefficients) for 60 min. The optimized process flow was used to achieve a high bond strength of 1.7 J/m$^2$, which is comparable to the bond strength achieved by Tong and Gösele after an annealing time of 100 hours at 300 °C. Likewise, the bond strength is almost equal to that

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The optimized bonding process was adapted to wafer bonding of (a) InP to SiO$_2$ and (b) GaAs to sapphire. The images show the bonded wafers after a complete III-V substrate removal. The un-bonded regions arise from particles introduced before and during the pre-bonding step.

achieved by Maszara et al. after annealing direct bonded Si wafers at around 1200 °C.

The optimized process was adapted to two hetero-material systems: InP bonded to SiO$_2$/Si and GaAs bonded to sapphire. Figure 7 shows the bonded samples after removal of the III-V substrate. The small un-bonded regions that are visible on the wafers are due to particles from handling of the wafers.

5. CONCLUSION

We have studied and optimized a low-temperature bonding process, that use Al$_2$O$_3$ as an intermediate layer for bonding of hetero-material systems. The process avoids any activation and surface treatment steps thus minimizing handling before bonding. A high bond strength of 1.7 J/m$^2$ was achieved for silicon wafers bonded using the Al$_2$O$_3$ intermediate layer. The optimized process was also adapted to bond III-V based hetero-material systems. The new bonding process is expected to enable novel nano-photonic devices in the future.

ACKNOWLEDGMENTS

The authors acknowledge the financial support from the Danish Innovation Foundation through the HERON project, the Villum Center of Excellence NATEC, and the National Basic Research Foundation centre SPOC (DNRF123). Aurimas Sakanas is acknowledged for providing the image of InP bonded to Si/SiO$_2$ in Figure 7.

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