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Published in:
Renewable Energy

Link to article, DOI:
[10.1016/j.renene.2014.10.026](https://doi.org/10.1016/j.renene.2014.10.026)

Publication date:
2015

Document Version
Peer reviewed version

[Link back to DTU Orbit](#)

Citation (APA):

Kong, W., Perers, B., Fan, J., Furbo, S., & Bava, F. (2015). A new Laplace transformation method for dynamic testing of solar collectors. *Renewable Energy*, 75, 448-458. DOI: 10.1016/j.renene.2014.10.026

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A new Laplace transformation method for dynamic testing of solar collectors

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Abstract

A new dynamic method for solar collector testing is developed. It is characterized by using the Laplace transformation technique to solve the differential governing equation. The new method was inspired by the so called New Dynamic Method (NDM) [1] but totally different. By integration of the Laplace transformation technique with the Quasi Dynamic Test (QDT) model [2], the Laplace – QDT (L-QDT) model is derived. Two experimental methods are then introduced. One is the shielding method which needs to shield and un-shield solar collector continuously during test period. The other is the natural test method which doesn't need any intervention.

The new L-QDT model with the shielding method are tested by TRNSYS [3] simulation. Experiments were carried out at Technical University of Denmark by using the L-QDT method and the natural experimental method. The identified collector parameters are then compared and analyzed with those obtained by the steady state test method and the QDT test method. The results comparison shows that the L-QDT method and the natural experimental method are also valid.

It can be concluded that the new Laplace test method can obtain reasonable and accurate collector parameters under transient weather condition.

Key words: solar collector, Laplace transformation technique, dynamic test method, solar collector parameters.

Nomenclature

A_p	Aperture area of solar collector (m^2)
c	Specific heat capacity ($J/(kg \cdot K)$)
F'	Collector efficiency factor (-)
$F'U_L$	Heat loss coefficient at $T_f - T_a = 0$ ($W/(m^2 \cdot K)$)

$F'U_1$	Temperature dependence of the heat loss coefficient ($W/(m^2 \cdot K^2)$)
$F'U_w$	Wind speed dependence of the heat loss coefficient ($J/(m^3 \cdot K)$)
G_t	Total solar irradiance (W/m^2)
G_b	Beam irradiance (W/m^2)
G_d	Diffuse solar irradiance (W/m^2)
K_b	Incident angle modifier for beam irradiance (-)
K_d	Incident angle modifier for diffuse irradiance (-)
L	Length of collector absorber (m)
m	Mass (kg)
\dot{m}	Mass flow rate (kg/s)
$(mc)_e$	Effective heat capacity of the collector per unit area ($J/(m^2 \cdot K)$)
n	Number of times
t	Time (s)
q_u	Heat flux per square meter (W/m^2)
T	Temperature (K)
T_m^*	Reduced temperature ($K \cdot m^2 / W$)
U	Heat loss coefficient ($W/(m^2 \cdot K)$)
w	Wind velocity (m/s)

Greek symbols

$\Delta\tau$	Time interval (s)
τ	Time (s)
$(\tau\alpha)_{en}$	Transmittance-absorptance product at normal incidence (-)
θ	Angle of incident (°)
ρ	Fluid density (kg/m^3)

Subscripts

a	Ambient
c	Collector

f	Fluid
fin	Collector absorber fin
fo	Fluid outlet
fi	Fluid inlet
w	Wind
0	Beginning

1. Introduction

1.1 Background

The solar collector testing technology is mainly applied in the area of solar collector evaluation and thermal performance prediction. The definition and identification of solar collector parameters are the main tasks of solar collector testing. The collector parameters can have a variety forms by different test methods. The prevalent test method is the steady state test method which is adopted by most test standards around the world such as ISO 9806 [4], EN 12975-2 [5] and ASHRAE 93 [6]. The steady state test method is featured by its simple mathematical model and convenient data processing method. But the strict test conditions and high-precision data acquisition requirements limit its wide application in connection with outdoor testing. For example, in some regions, especially the north of Europe, it may take several months to acquire enough test data for one test. What's more, the cost of construction and maintenance of the high-precision data acquisition device and control instruments will be obviously high.

To overcome the drawbacks of the steady state test method mentioned above, different kinds of dynamic and quasi-dynamic test methods have been invented since 1980s [7]. Generally, the dynamic test method can be characterized by its relatively complicated mathematical model and data processing techniques but relatively loose test conditions, short test period and extensive adaptability. The Quasi-Dynamic Test (QDT) method [2] is the only dynamic test method adopted by the standard till now as an alternative method in EN 12975 [5] and ISO 9806 [4]. It is the representative of one node method which considers the solar collector and the fluid as a whole. The collector thermal capacity is lumped together and referenced by the mean fluid temperature. The transfer function method [8-11] and the improved transfer function (ITF) method [12] are typical multi-node test methods. The solar collector is divided into a solid part and a fluid part. Each part has its own thermal capacity which is referenced

by each part's mean temperature. Other dynamic test methods are known as its unique mathematical model or data processing techniques such as response function method [13-16], the filter method [17], the Laplace transformation method [1], the thermal resistance method [18], the power correction method [19], etc.

1.2 The Quasi-Dynamic Test (QDT) method

The QDT method [20-22] was first developed by Bengt Perers in 1990 and adopted by the European standard EN 12975 [5] in 2000 and by the international standard ISO 9806 [4] in 2013. The QDT mathematical model is well known as Eq. (1). The left hand side of Eq. (1) is solar collector's effective power gain. While at the right hand side, the irradiance is divided into the beam and the diffuse term each with its incident angle modifier and the rest are the detailed heat losses terms. The accuracy of the QDT method has been validated by different independent research, see [7].

$$\begin{aligned} qu = \dot{m}c_f(T_{fo} - T_{fi}) / A_p = F'(\tau\alpha)_{en}K_bG_b + F'(\tau\alpha)_{en}K_dG_d - F'U_L(T_f - T_a) \\ - F'U_1(T_f - T_a)^2 - F'U_{ww}(T_f - T_a) - (mc)_e \frac{dT_f}{dt} \end{aligned} \quad (1)$$

Compared with the steady state test method, most of the test conditions are loosened in the QDT method. But the allowed deviation of the inlet temperature is still strictly restricted within ± 1 K during one test sequence and the flowrate should also be constant. The test duration is usually the same with the steady state test method and it was reported that the thermal capacity of solar collector may not always accurately be identified since the collector reacts under constant inlet temperature condition which could not supply enough collector dynamic response information [23].

1.3 The New Dynamic Method (NDM)

Amer and Nayak [1, 24] developed a new dynamic method (NDM) which is characterized by using the Laplace transformation method for the mathematical model development.

The NDM method is summarized as follows [1]. Consider an element of length Δx along the flow direction of the collector. Its width w equals to the length between the axes of two adjacent riser tubes. The energy balance equation for the element at any time can be expressed as

$$\dot{m}c_f[T_f(x + \Delta x, \tau) - T_f(x, \tau)] = F'(\tau\alpha)_{en}G_i(\tau)w\Delta x - F'U_L[T_f(x, \tau) - T_a(\tau)]w\Delta x - (mc)_{\Delta x} \frac{dT_f(x, \tau)}{d\tau} \quad (2)$$

The effective thermal capacitance of the collector is considered to be uniformly distributed over the area of the collector, then

$$\frac{(mc)_{\Delta x}}{w\Delta x} = \frac{(mc)_{fin}}{wL} = \frac{(mc)_e}{A_p} \quad (3)$$

Take limit of Eq. (2) can derive

$$\frac{\partial T_f(x, \tau)}{\partial x} + \frac{F'U_L A_p}{\dot{m}c_f L} T_f(x, \tau) = \frac{F'(\tau\alpha)_{en} A_p}{\dot{m}c_f L} G_i(\tau) + \frac{F'U_L A_p}{\dot{m}c_f L} T_a(\tau) - \frac{(mc)_e}{\dot{m}c_f L} \frac{\partial T_f(x, \tau)}{\partial \tau} \quad (4)$$

The initial and boundary conditions are

$$T_f(x, 0) = T_0 \quad (5)$$

$$T_f(0, t) = T_{fi}(t) \quad (6)$$

Eq. (4) is solved by using the Laplace transformation technique which gives the final expression of the fluid mean temperature

$$\begin{aligned} T_f(x, \tau) = & \int_0^\tau \left[\frac{F'(\tau\alpha)_{en}}{(mc)_e} G_i(\tau-t) + \frac{F'U_L}{(mc)_e} T_a(\tau-t) \right] \exp\left(\frac{F'U_L}{(mc)_e} t\right) dt \\ & + T_0 \exp\left(-\frac{F'U_L}{(mc)_e} \tau\right) \left[1 - u\left(\tau - \frac{\tau_d x}{L}\right) \right] + \exp\left(-\frac{\tau_d x}{\tau_L L}\right) \left[T_{fi}\left(\tau - \frac{\tau_d x}{L}\right) u\left(\tau - \frac{\tau_d x}{L}\right) \right] \\ & - \int_0^\tau \left[\frac{F'(\tau\alpha)_{en}}{(mc)_e} G_i(\tau-t) + \frac{F'U_L}{(mc)_e} T_a(\tau-t) \right] \exp\left(\frac{F'U_L}{(mc)_e} t\right) u\left(t - \frac{\tau_d x}{L}\right) dt \end{aligned} \quad (7)$$

Where

$$\tau_d = \frac{(mc)_e}{\dot{m}c_p} \quad (8)$$

$$\tau_L = \frac{(mc)_e}{F'U_L} \quad (9)$$

and $u\left(t - \frac{\tau_d x}{L}\right)$ is the unit step function.

As for a transient process from time zero to τ_d and x equals to L , Eq. (7) can be simplified to express the outlet temperature at the end of transient period and can be rewritten as

$$T_{fo}(\tau) = \int_0^{\tau_d} \left[\frac{F'(\tau\alpha)_{en}}{(mc)_e} G_i(\tau-t) + \frac{F'U_L}{(mc)_e} T_a(\tau-t) \right] \exp\left(\frac{F'U_L}{(mc)_e} t\right) dt + T_0 \exp\left(\frac{F'U_L}{(mc)_e} \tau\right) \quad (10)$$

The right hand side of Eq. (10) consists of two terms. The first term represents the environmental conditions which can be interpreted as the input influence to the collector. The other term means the initial effect to the outlet temperature. The exponential function in both terms means the weighting factor of the effect contributing to the dynamic changes of temperature of each time step during transient operations.

The integral equation can be discretized into Eq. (11) after the response time τ_d is divided into N equal time segments. The environmental inputs at each of $\Delta\tau$ time step contribute to the final outlet temperature. τ_d is chosen as the response of the collector to any transient input would reach 95% of the final steady state value.

$$T_{fo}(\tau_d) = T_0 \exp\left(\frac{F'U_L}{(mc)_e} \tau_d\right) + \sum_{k=0}^{n-1} \left[\frac{F'(\tau\alpha)_{en}}{(mc)_e} G_i(\tau_d - k\Delta\tau) + \frac{F'U_L}{(mc)_e} T_a(\tau_d - k\Delta\tau) \right] \exp\left(\frac{F'U_L}{(mc)_e} k\Delta\tau\right) \Delta t \quad (11)$$

Eq. (11) is a non-linear equation containing three unknown parameters $F'(\tau\alpha)_{en}$, $F'U_L$ and $(mc)_e$. A standard optimization routine from [25] was recommended to obtain the three collector parameters.

The experimental method is similar to the time constant test. The solar collector is shielded by an opaque or semi-transparent shield for some time and then exposed to the sun for some time. These shielding and un-shielding experiments are implemented during all test period and the experimental data are then collected during these repeated activities.

It is shown in the paper [1] that the NDM method can give accurate and stable results and has high precision which is comparable with steady state test method. But the paper is still missing information on the detailed process for deriving the mathematical model and has no introduction of the computational method for the non-linear equation and no specific description of how to select and process test data. In addition, the derivation process of the mathematical model of the NDM method is relatively complicated and only three collector parameters have no advantage compared to the steady state test method.

In this paper a new dynamic test method based on the QDT mathematical model and the Laplace transformation techniques is developed. The new Laplace method is simpler in mathematical model derivation than the NDM method but contains more meaningful collector parameters. Two experimental methods and data processing method are specified. TRNSYS [3] simulation and experiments verification are also carried out for the two experimental methods. The results comparison shows that the new Laplace transformation method can obtain accurate collector parameters under transient weather conditions in solar collector testing area.

2. The new Laplace transformation method

2.1 Mathematical model

Considering a transient response process of a solar collector, the basic dynamic energy conservation equation Eq. (12) can be used as the governing equation. It has the same mathematical structure as the QDT model of Eq. (1).

$$qu = \dot{m}c_f(T_{fo} - T_{fi}) / A_p = F'(\tau\alpha)_{en}G_t - F'U_L(T_f - T_a) - (mc)_e \frac{dT_f}{dt} \quad (12)$$

All the variables in Eq. (12) are the function of time. For simplicity's sake, set the equation parameters to simple symbols - $\dot{m}c_f/A_p = A$, $F'(\tau\alpha)_{en} = B$, $F'U_L = C$, $(mc)_e = D$.

By rearranging Eq. (12), the simplified governing equation is

$$D \frac{dT_f}{dt} = BG_t - C(T_f - T_a) - A(T_{fo} - T_{fi}) \quad (13)$$

The Laplace transformation technique used for both sides of Eq. (13) gives Eq. (14).

$$(Ds + C)T_f(s) = BG_t(s) + CT_a(s) - AT_{fo}(s) + AT_{fi}(s) + DT_f(0) \quad (14)$$

The mean fluid temperature $T_f(s)$ in the Laplace space can be expressed as

$$\begin{aligned} T_f(s) &= \frac{BG_t(s) + CT_a(s) - AT_{fo}(s) + AT_{fi}(s) + DT_f(0)}{Ds + C} \\ &= \frac{1}{s + \frac{C}{D}} \left[\frac{B}{D}G_t(s) + \frac{C}{D}T_a(s) - \frac{A}{D}T_{fo}(s) + \frac{A}{D}T_{fi}(s) + T_f(0) \right] \end{aligned} \quad (15)$$

Then the inverse Laplace transformation technique was applied to Eq. (15) and the final analytical solution of the mean fluid temperature $T_f(t)$ in the time space can be obtained as the following equation.

$$\begin{aligned} T_f(\tau) &= \int_0^\tau \left\{ \frac{F'(\tau\alpha)_{en}}{(mc)_e} G_t(\tau - t) + \frac{F'U_L}{(mc)_e} T_a(\tau - t) - \frac{\dot{m}c_f}{(mc)_e A_p} [T_{fo}(\tau - t) - T_{fi}(\tau - t)] \right\} \exp\left(-\frac{F'U_L}{(mc)_e} t\right) dt \\ &\quad + T_f(0) \exp\left(-\frac{F'U_L}{(mc)_e} \tau\right) \end{aligned} \quad (16)$$

Eq. (16) is an integral non-linear equation which has clear mathematical structure and physical meaning. It can be explained as the following way. For a period (0- τ), the mean fluid temperature of a solar collector at the end time $T_f(\tau)$ equals to the initial effect of the mean fluid temperature at the beginning time $T_f(0)$ and the summation influence of the environmental parameters (G_t , T_a , T_{fo} , T_{fi} , \dot{m}) during the period of (0- τ). Each term has its own exponential function as the weighting factor to determine how much it contributes to the final mean temperature.

Eq. (16) contains three undetermined collector parameters $F'(\tau\alpha)_{en}$, $F'U_L$ and $(mc)_e$. But the Laplace and the reverse Laplace derivation method can be easily applied to the QDT model because Eq.

(1) and Eq. (12) have the same mathematical structure. The QDT model contains more meaningful collector parameters than Eq. (12). By applying the Laplace and reverse Laplace transformation treatment for the QDT model, the L-QDT (Laplace QDT) mathematical model can be obtained as

$$T_f(\tau) = \int_0^\tau \left\{ \frac{F'(\tau\alpha)_{en}}{(mc)_e} G_b(\tau-t) - \frac{F'(\tau\alpha)_{en} \cdot b_0}{(mc)_e} \left(\frac{1}{\cos(\theta)} - 1 \right) G_b(\tau-t) + \frac{F'(\tau\alpha)_{en} K_d}{(mc)_e} G_d(\tau-t) + \frac{F'U_L}{(mc)_e} T_a(\tau-t) \right. \\ \left. - \frac{\dot{m}c_f}{(mc)_e A_p} [T_{f_o}(\tau-t) - T_{f_i}(\tau-t)] - \frac{F'U_1}{(mc)_e} T_1(\tau-t) - \frac{F'U_w}{(mc)_e} T_2(\tau-t) \right\} \exp\left(-\frac{F'U_L}{(mc)_e} t\right) dt \\ + T_f(0) \exp\left(-\frac{F'U_L}{(mc)_e} \tau\right) \quad (17)$$

Where

$$T_1(t) = [T_f(t) - T_a(t)]^2 \quad (18)$$

$$T_2(t) = [T_f(t) - T_a(t)] \cdot w(t) \quad (19)$$

In Eq. (17), the beam incident angle modifier K_b is modeled as the b_0 equation which is shown in Eq. (20). Another alternative is the so called angle by angle method developed by Perers [21]. Or it can be called the extended MLR method in [2]. The beam irradiance in the collector plane is sorted into different columns based on the average incident angle. For example 10° is chosen as the interval between the columns. Using higher angular resolution can get higher accuracy. The multi linear regression [12] and the non-linear regression can both use this method to get a set of collector efficiencies angle by angle together with the other collector parameters. The efficiencies under different incident angles can be obtained without any pre-determined models.

$$K_b(\theta) = 1 - b_0 \left[\frac{1}{\cos(\theta)} - 1 \right] \quad (20)$$

2.2 Discretization of the integral equation

The integral expression of Eq. (16) should be discrete in the practical use. The period of a dynamic response process of solar collector from 0 to τ_d is considered. τ_d can be divided into n time intervals. Each time interval is Δt , therefore $n\Delta t = \tau_d$.

The discrete format of Eq. (16) is

$$T_f(\tau_d) = T_f(0) \exp\left(-\frac{F'U_L}{(mc)_e} \tau_d\right) + \sum_{k=0}^{n-1} M(\tau_d - k\Delta t) \exp\left(-\frac{F'U_L}{(mc)_e} k\Delta t\right) \Delta t \quad (21)$$

Where

$$M(t) = \frac{F'(\tau\alpha)_{en}}{(mc)_e} G_t(t) + \frac{F'U_L}{(mc)_e} T_a(t) - \frac{\dot{m}c_f}{(mc)_e A_p} [T_{f_o}(t) - T_{f_i}(t)] \quad (22)$$

The same discrete method can also be used in the mathematical model of the L-QDT method of Eq. (17). The theory is the same while the only difference is that the L-QDT model contains more collector parameters.

A simple example will be enough to illustrate the essence of this Laplace method and the discrete mathematical model of Eq. (21). A typical dynamic response process of a solar collector can be seen in Fig. 1 which shows the collector mean fluid temperature T_f decreases with time. The time interval of each point is 2 s. For simplicity, 4 nodes are chosen to represent the whole dynamic process. The first node is labeled as $t=1$ indicating the beginning of the dynamic process while the last node is marked as $t=4$ representing the end. Therefore totally $3\Delta t$ time intervals are identified. Then the discrete format of Eq. (21) can be expressed as Eq. (23).

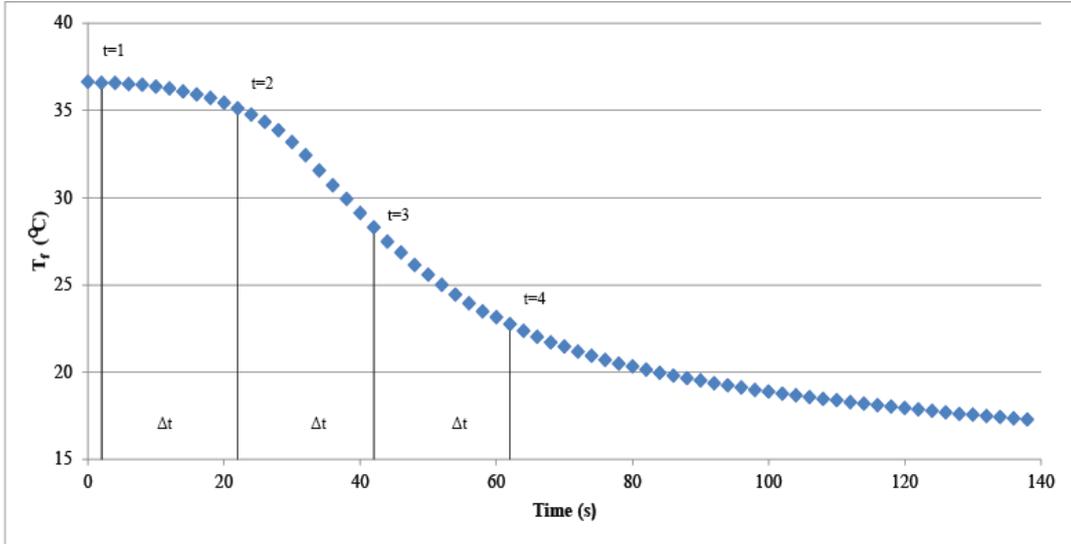


Fig. 1. Simplified 4 nodes example of a full response dynamic process of a solar collector

$$\begin{aligned}
T_f(4) = & T_f(1) \exp\left(-\frac{F'U_L}{(mc)_e} 3\Delta t\right) \\
& + \left\{ \frac{F'(\tau\alpha)_{en}}{(mc)_e} G_i(2) + \frac{F'U_L}{(mc)_e} T_a(2) - \frac{\dot{m}c_f}{(mc)_e A_p} [T_{fo}(2) - T_{fi}(2)] \right\} \exp\left(-\frac{F'U_L}{(mc)_e} 2\Delta t\right) \Delta t \\
& + \left\{ \frac{F'(\tau\alpha)_{en}}{(mc)_e} G_i(3) + \frac{F'U_L}{(mc)_e} T_a(3) - \frac{\dot{m}c_f}{(mc)_e A_p} [T_{fo}(3) - T_{fi}(3)] \right\} \exp\left(-\frac{F'U_L}{(mc)_e} 1\Delta t\right) \Delta t \\
& + \left\{ \frac{F'(\tau\alpha)_{en}}{(mc)_e} G_i(4) + \frac{F'U_L}{(mc)_e} T_a(4) - \frac{\dot{m}c_f}{(mc)_e A_p} [T_{fo}(4) - T_{fi}(4)] \right\} \exp\left(-\frac{F'U_L}{(mc)_e} 0\Delta t\right) \Delta t
\end{aligned} \quad (23)$$

The mathematical structure and physical meaning of Eq. (23) is also clear. For a dynamic response process, the collector final mean temperature $T_f(4)$ is determined by the initial mean temperature $T_f(1)$ and the historical environmental parameters. All the suitable dynamic response process will be selected from the raw data and used for identifying the collector parameters.

Eq. (23) is a non-linear equation. The non-linear regression or the optimization method can be used for identifying the undetermined collector parameters. Standard programs of the two methods can be easily found in the math softwares such as Matlab [26] and R [27]. The difference between the non-linear regression method and the multi-linear regression method (MLR) is that the non-linear regression needs the initial values for the undetermined parameters. But as long as the governing equation and the test data are correct, the final results will be the same no matter what kind of non-linear regression method or initial values are used.

3. Experimental test method

Two experimental test methods are introduced in the following sections. One is an artificial intervention method which can be called the shielding method. This method creates dynamic response test data by shielding and un-shielding solar collectors. The other is the so called natural test method which does not need special manual intervention, just records and selects suitable test data from the routine solar collector test.

3.1 The shielding and un-shielding experimental test method

An opaque or semi-transparent cloth or board is used to shield the solar collector and pyranometer from sun light. It is recommended from the literature [1] that the irradiance measured by the shielded pyranometer should be less than 20% of total irradiance. Of course the best situation is that the cloth or board can block all the irradiance. The shield should be placed in parallel of the collector surface at a height of about 0.5 m. The area of the shield is bigger than the collector area such that it extends beyond the collector edges by 0.5 m from all four sides.

The duration of shielding and un-shielding should be longer than two times of the collector time constant in order to achieve the full dynamic response data of solar collector. The purpose of shielding and un-shielding action is to create the collector dynamic response process artificially. Sufficient long shielding and un-shielding duration is the guarantee of a full dynamic reaction for solar collectors. According to the shielding theory above and the TRNSYS simulation results in section 4, this artificial intervention method can create useful dynamic response process as much as possible. Therefore, this shielding and un-shielding method can greatly save time in experiments.

Another important thing is the varying inlet temperature. It has been found that the inlet temperature should present considerable change through testing otherwise the heat loss factor as well as the thermal

capacity of solar collector will not be properly estimated [23]. It is recommended that the inlet temperature varies from ambient temperature to the highest possible collector temperature if the test conditions allows.

Figs. 3-5 show the ideal shielding and un-shielding irradiance conditions which were created by TRNSYS.

3.2 The natural experimental test method

The natural experimental test method is free of the shielding and un-shielding actions. The only thing is to record all the variations of the collector parameters. The method based on the theory that the transient weather conditions can also create natural shielding and un-shielding effects during collector test. For example when the clouds pass over a solar collector, the shielding effect will be created while when the clouds leave away, the solar collector will react as the un-shielding condition. Then after the test, the suitable dynamic test data will be selected according to the following rules. Assume that the collector full response time is T . T can be determined by the following test procedure - the collector is shielded from the sun in a steady state and then exposed to the sun until it reaches another steady state after removing the shielding. Or the collector is exposed to the sun in a steady state and then it is shielded until reaching another steady state. The time period between the two steady state conditions is the full response time T and the 63.2% T is defined as T_C . Therefore the test data in which the collector response time lies between T_C and T is chosen for identifying collector parameters. The method is verified in section 5.

The two methods give different lengths of the mathematical model of Eq. (21). The shielding and un-shielding actions make fully reacted collector response processes therefore all the dynamic data substituted into Eq. (21) has full response time T while the natural experimental test data contains all kinds of collector response processes such as steady state data, fully reacted data, and of course most of them are partial dynamic response data. Only the data in which the response time lies from T_C to T will be selected.

A typical schematic diagram of the natural experimental test is shown in Fig. 2. The mean fluid temperature T_f varies with time under transient environmental conditions. From Fig. 2 it can be seen that the T_f descending region caused by the total irradiance decrease corresponding to the shielding process and the T_f rising region caused by the total irradiance increase corresponding to the un-shielding process.

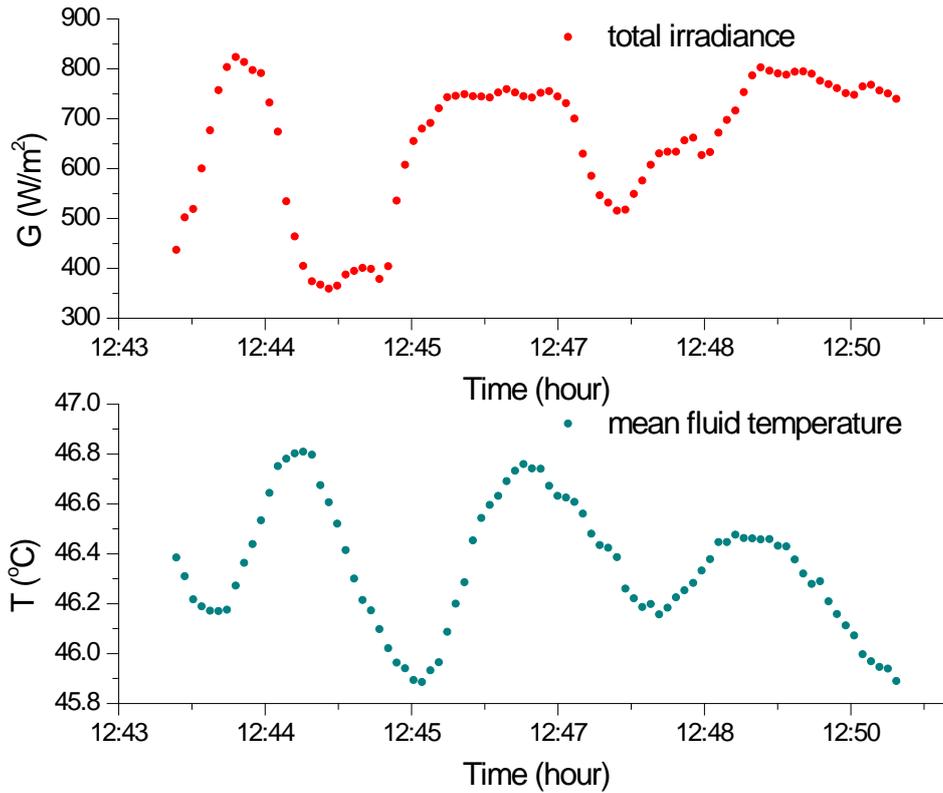


Fig. 2. A typical varying profile of mean fluid temperature under natural weather condition

4 TRNSYS simulation for the shielding experimental method

Theoretical calculations by using the shielding test method were carried out in TRNSYS simulation studio. The validated Type 832 solar collector model [28] was chosen to simulate the dynamic behavior of a flat plate solar collector under the DK-Kobenhavn-Taastrup weather data provided by TRNSYS 17. Three test days are chosen arbitrarily and the solar irradiance was processed by equation module to simulate the shielding and un-shielding effect. The weather conditions are plotted in Fig. 3 to Fig. 5. The setting values of the collector parameters are listed in Table 1. The duration of shielding and un-shielding action is 7.5 min which is long enough for the dynamic response of the solar collector. Two data acquisition time of 5 s and 10 s with 72 kg/h constant flow rate was set for the simulation test. The inlet temperature was designed to vary in sine profile between the ambient temperature and 90 °C.

Table 1 The setting values of collector parameters in TRNSYS

Symbol	Collector parameter	Value	Unit
A_p	Collector aperture area	1	m^2
$F(\tau\alpha)_{en}$	Zero loss efficiency	0.7	-
b_0	IAM parameter for beam radiation	0.2	-
K_d	IAM for diffuse radiation	0.9	-
FU_L	Linear heat loss coefficient	3	W/m^2K
FU_1	Quadra heat loss coefficient	0.01	W/m^2K^2
FU_w	wind loss coefficient	0.1	J/m^3K
$(mc)_d$	thermal capacity for the solid part	5000	J/m^2K
$(mc)_f$	thermal capacity for the fluid part	1500	J/m^2K

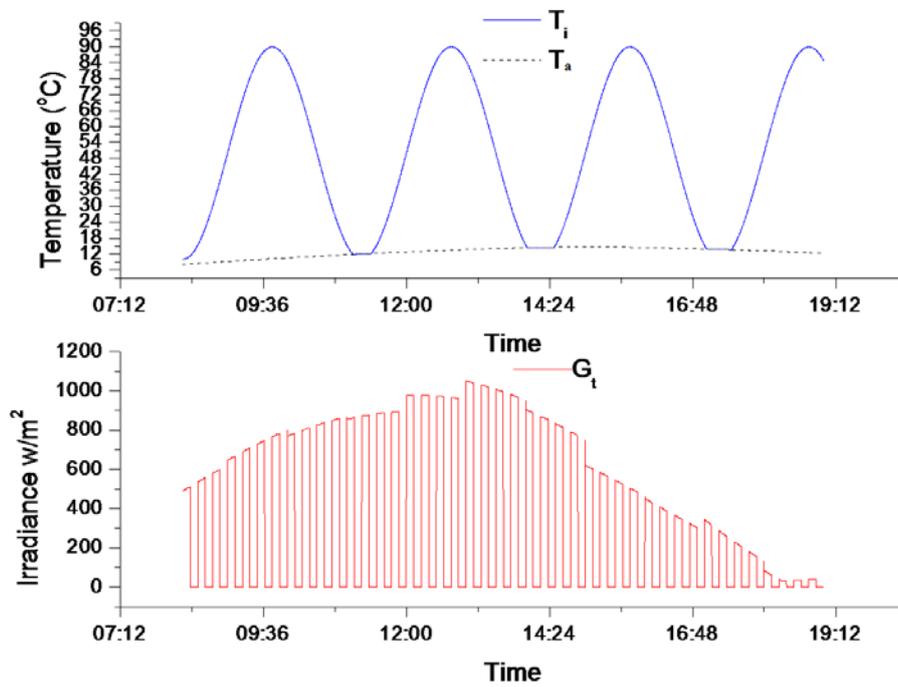


Fig. 3 The test condition of 1st of May

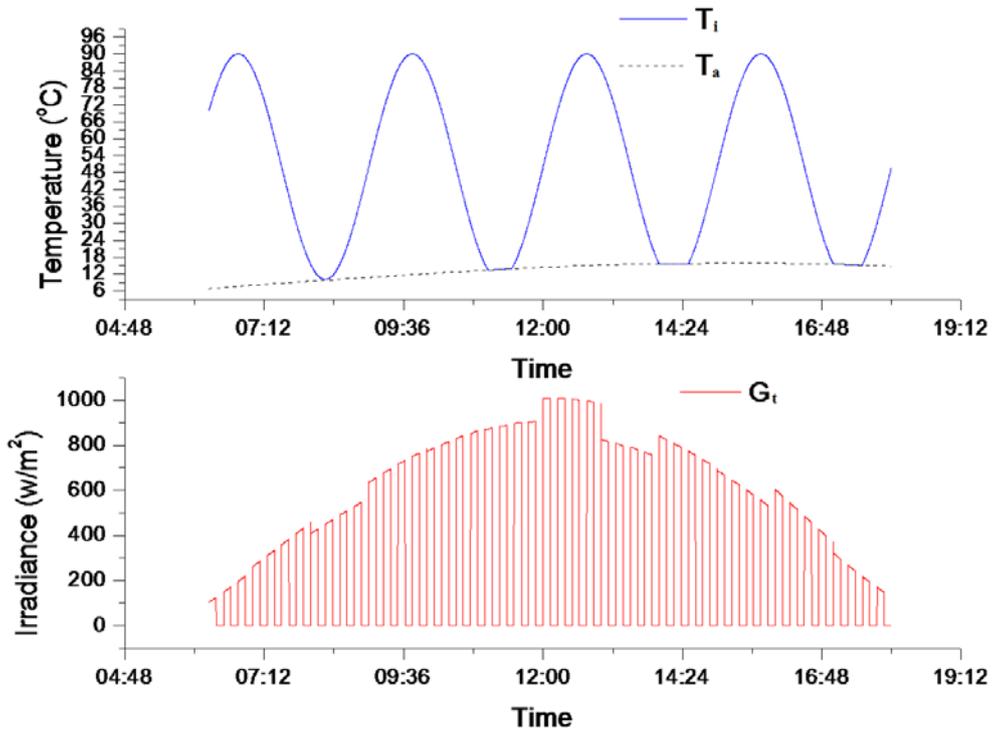


Fig. 4 The test condition of 2nd of May

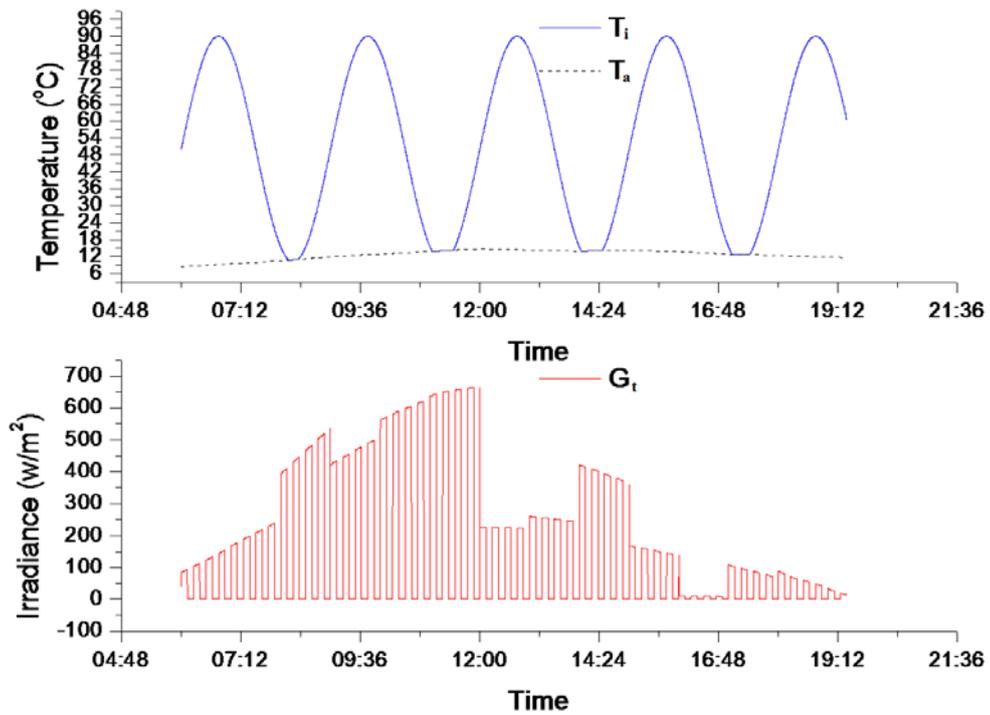


Fig. 5 The test condition of 3rd of May

Table 2 Comparison of collector parameters under different test conditions

Parameters	Setting value	Data acquisition time interval	
		5 s	10 s
$F'(\tau\alpha)_{en}$	0.7	0.66(5.7%)	0.67(4.3%)
b_0	0.2	0.20(0%)	0.25(25%)
K_d	0.9	0.90(0%)	0.92(2.2%)
$F'U_L$	3	2.80(6.7%)	2.90(3.3%)
$F'U_1$	0.01	0.02(100%)	0.013(30%)
$F'U_w$	0.1	0.08(20%)	0.09(10%)
$(mc)_e$	6500	6740(3.7%)	6701(3.1%)

The collector parameters are identified by using the simulated test data and compared with the setting values which are shown in Table 2. The relative error of each collector parameter is illustrated in the bracket which is defined as $|P_{calculated} - P_{setting}|/P_{setting}$. It can be seen from Table 2 that all the collector parameters are successfully obtained and the results are close to the setting values except the quadratic heat loss coefficient $F'U_1$. The relative error of the zero loss coefficient $F'(\tau\alpha)_{en}$, the heat loss coefficient $F'U_L$ and the collector thermal capacity $(mc)_e$ are all under 7%. The largest relative error comes from the quadratic heat loss coefficient $F'U_1$. But the value of itself is very small and won't significantly affect the efficiency and energy output. Therefore the regression process can be considered successful.

5. Experimental verification for the natural test method

5.1 Test platform and solar collector

A flat plate solar collector was tested at the Technical University of Denmark on 18 June and 02-04 July 2014. The solar collector is designed for medium and large solar heating system with the gross area of 13.53 m² and the aperture area of 12.56 m². There is a transparent ETFE (Ethylene tetrafluoroethylene) foil equipped between the absorber and the surface glass with the aim to reduce the convection heat loss. Water was used as the working fluid.

The solar collector photograph and schematic diagram of the test rig are shown in Fig. 6 and Fig. 7

respectively. Data of the test rig facilities are listed in Table 3. The slope of the test solar collector is 45° . The collector fluid is pumped through the solar collector with the fluid flow rate of 25 l/min during the whole test period. The fluid inlet temperature was controlled by the electrical heating and water cooling devices to make sure that it can vary during test. There were no requirements for weather conditions. All the data including the total irradiance (G_t), the diffuse irradiance (G_d), the ambient temperature (T_a), the fluid inlet and outlet temperature (T_{fi} and T_{fo}) and the fluid flow rate (\dot{m}) were recorded by the data logger. The time interval of data acquisition is 10 s.



Fig. 6 Photograph of solar collector

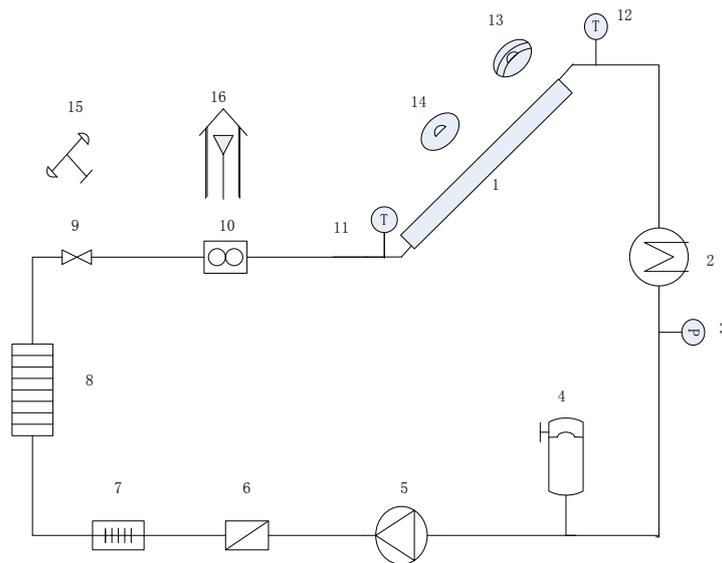


Fig. 7 Test rig schematic

Table 3 Test rig facilities

No.	Facility	No.	Facility
1	Solar collector	9	Flow control valve
2	Primary temperature regulator	10	Flow meter
3	Pressure gauge	11	Inlet temperature sensor
4	Expansion tank	12	Outlet temperature sensor
5	Pump	13	Pyranometer with shadow band
6	Filter	14	Pyranometer
7	Electric heater	15	Anemometer
8	Secondary temperature regulator	16	Ambient temperature sensor

5.2 Test conditions

The measurement data of the test period is shown below. The total and diffuse irradiance is illustrated in Fig. 8. The profile of the fluid inlet temperature and the ambient temperature can be seen in Fig. 9.

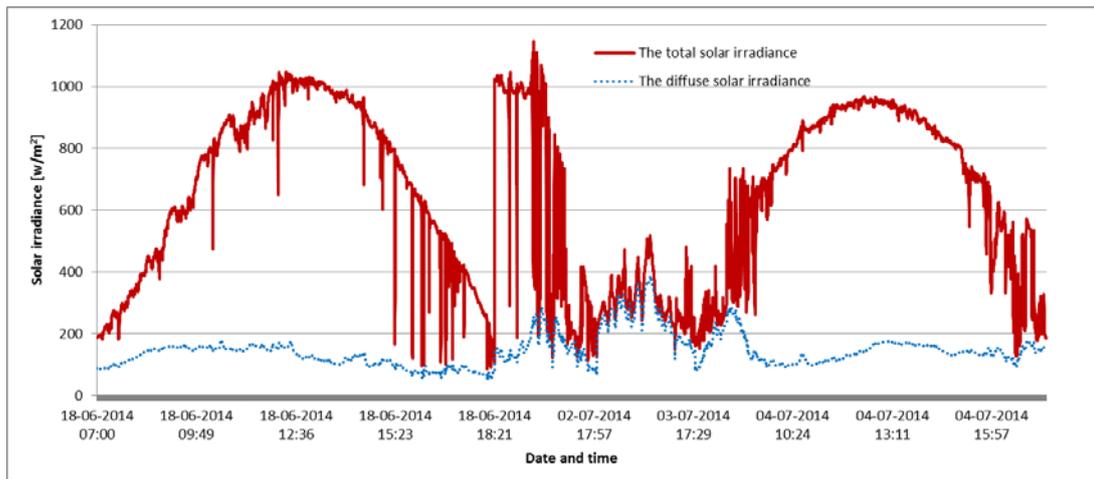


Fig. 8 The total and diffuse irradiance on collector surface during test period

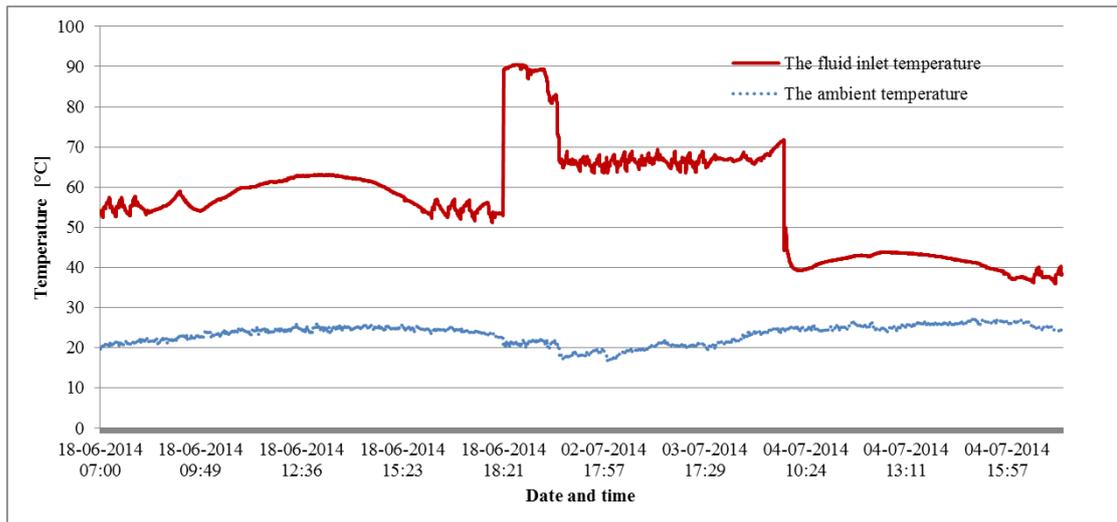


Fig. 9 The inlet temperature and ambient temperature during test period

It can be seen from Fig. 8 that the weather condition was unstable most of time. The drastic changing irradiance indicates that there were lots of crossing clouds during the test period. Actually, this cloud-crossing weather condition has similar effect as the collector shielding and un-shielding actions. Therefore the test data contains the collector's dynamic response information which can be used to calculate the collector's parameters.

5.3 Results and discussion

The suitable L-QDT test data were selected from the raw data to identify the collector parameters. All the data processing, non-linear regression and statistics analysis were carried out at the R platform [27]. The steady state test data and the QDT test data are chosen from the test data of June and July 2014 based on the criteria of EN 12975-2 [5].

The full dynamic response time of the tested solar collector is 108 s and the time constant is 68 s. The data acquisition time interval is 10 s. Then the suitable dynamic data length of the L-QDT method can be determined between 70 s and 110 s. Therefore the test data in which the dynamic response time is larger than 70 s and less than 110 s are chosen as useful data. In addition, the pretreatment for the raw data is also important for obtaining accurate results, such as the bad points removing and data filter technique [29]. It is noted that during the test period the shadow ring for measuring the diffuse irradiance was not well adjusted in the morning and the afternoon. Therefore the test data were filtered by the condition that the beam irradiance should be larger than 30 W/m^2 in order to remove the inaccurate diffuse irradiance.

The results of the model parameters with statistics are shown in Table 4. The collector parameters

calculated from Table 4 are shown in Table 5. The steady state test results, the QDT test results are also listed in the same table. The relative errors of the QDT and L-QDT method compared with the steady state results are present in the brackets.

It can be seen from Table 4 that the angle by angle method was used to describe the incident angle modifier (IAM) with the resolution of 15° . Fig. 10 shows the IAM comparison modelled by the L-QDT and the QDT angle by angle method and the b_0 equation of the steady state method. The b_0 value is obtained by modeling the efficiencies in Table 4 under different incident angles into the b_0 equation.

All the t values in Table 4 are larger than 2 indicates that the non-linear regression is valid and the estimated results are statistic reasonable.

From the results comparison of Table 5 it can be seen that the collector parameters identified by the L-QDT method are close to those obtained by the steady state method, especially the most important two collector parameters - the zero loss efficiency $F'(\tau\alpha)_{en}$ and the heat loss coefficient $F'U_L$. Both the $F'(\tau\alpha)_{en}$ and the $F'U_L$ have the relative errors less than 2%. The QDT method also gives close results compared to the steady state test method. But the relative errors of $F'(\tau\alpha)_{en}$ and $F'U_L$ are a little bit larger than that of the L-QDT method. The linear efficiency curves obtained by the steady state method, the QDT method and the L-QDT method can be seen in Fig. 11 which shows the instantaneous efficiencies curves of the L-QDT method and the steady state method are very close.

The quadratic heat loss coefficient $F'U_1$ has relative large difference by the two test methods compared with the steady state method. But it is due to the relatively "stable" inlet temperature which is lack of the information of the whole T_m^* region, especially the high inlet temperature. The limited test data gives a higher value of the $F'U_1$ which is reflected in the comparison of the quadratic efficiency curves in Fig. 12.

The b_0 value of the two methods also has relative large difference which is mainly caused by the filter condition of $G_b > 30 \text{ W/m}^2$. The filter condition is intended to eliminate the incorrect diffuse irradiance with the consequence of reducing the information of the high incident angle data which usually exist in the low beam irradiance condition. It is believed that the L-QDT and angle by angle method can give more accurate IAM results as long as sufficient test data provided.

In general the comparison shows that the natural experimental method can obtain reasonable collector parameters.

Table 4 Model parameters and statistics based on the L-QDT method

Coefficients	Estimate	Standard error	t value	P(> t)
$F'(\tau\alpha)_{(0^\circ-15^\circ)}$	8.175×10^{-1}	1.753×10^{-2}	46.643	$< 2 \times 10^{-16}$
$F'(\tau\alpha)_{(15^\circ-30^\circ)}$	7.946×10^{-1}	9.849×10^{-3}	80.675	$< 2 \times 10^{-16}$
$F'(\tau\alpha)_{(30^\circ-45^\circ)}$	7.948×10^{-1}	9.741×10^{-3}	81.591	$< 2 \times 10^{-16}$
$F'(\tau\alpha)_{(45^\circ-60^\circ)}$	7.354×10^{-1}	1.426×10^{-2}	51.560	$< 2 \times 10^{-16}$
$F'(\tau\alpha)_{(60^\circ-75^\circ)}$	5.628×10^{-1}	2.797×10^{-2}	20.123	$< 2 \times 10^{-16}$
$F'(\tau\alpha)_{(75^\circ-90^\circ)}$	3.368×10^{-1}	7.609×10^{-2}	4.427	1.28×10^{-5}
$F'U_L$	2.241	4.399×10^{-1}	5.095	5.74×10^{-7}
$F'(\tau\alpha)_{en} \cdot K_d$	8.099×10^{-1}	3.751×10^{-2}	21.591	$< 2 \times 10^{-16}$
$F'U_1$	2.202×10^{-2}	5.983×10^{-3}	3.681	2.69×10^{-3}
$(mc)_e$	5.405×10^3	2.086×10^2	25.913	$< 2 \times 10^{-16}$

Table 5 Collector parameters comparison based on the steady state, the QDT and the L-QDT method

Coefficients	$F'(\tau\alpha)_{en}$	b_0	K_d	$F'U_L$	$F'U_1$	$(mc)_e$
SST Estimate	0.817	0.14	-	2.210	0.014	-
QDT Estimate	0.800(2.1%)	0.18(28.6%)	0.97	2.155(2.5%)	0.022(57%)	4092
L-QDT Estimate	0.818(0.12%)	0.19(35.7%)	0.99	2.241(1.4%)	0.022(57%)	5405

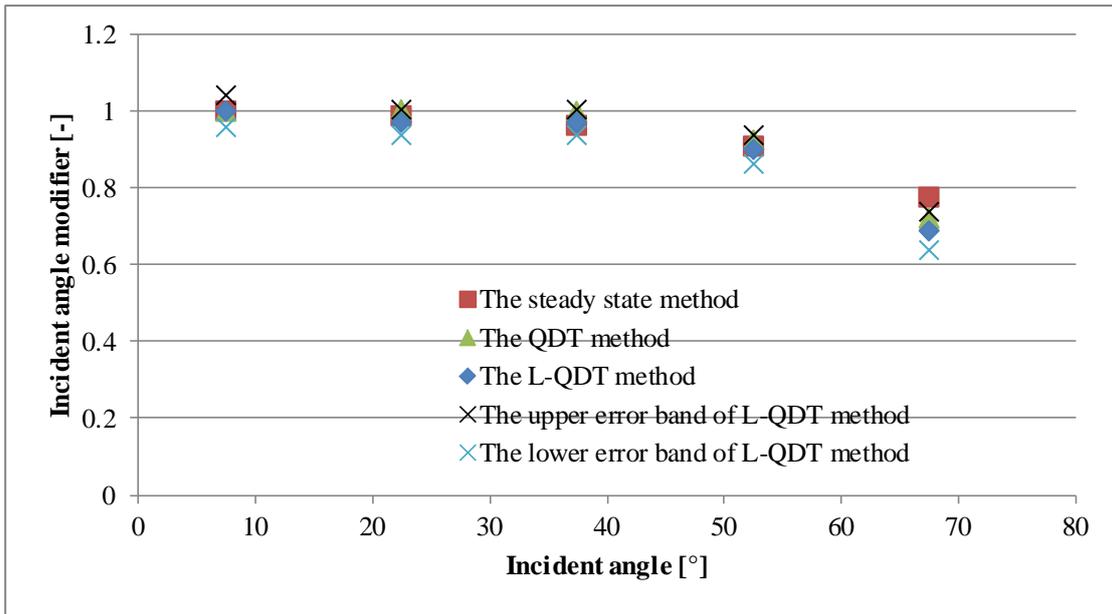


Fig. 10 The comparison of incident angle modifier by using the steady state, the QDT and the L-QDT method

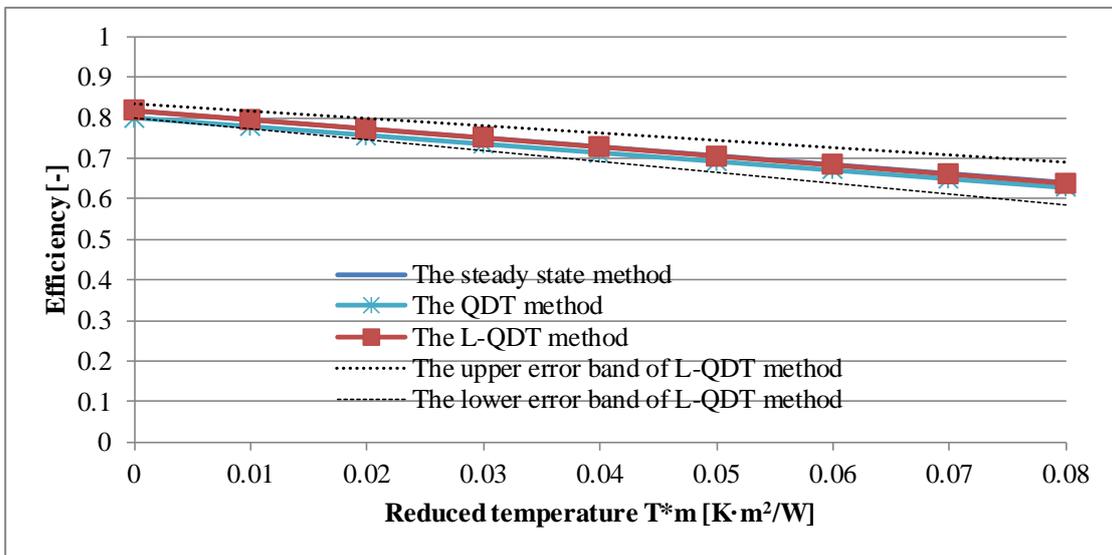


Fig. 11 The comparison of the linear efficiency curves by using the steady state, the QDT and the L-QDT method

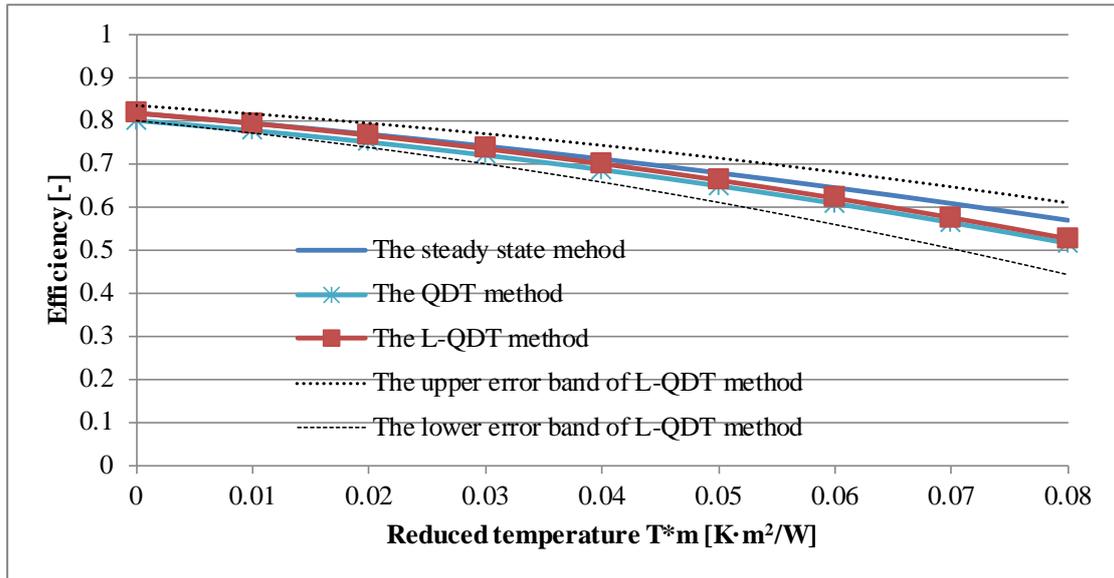


Fig. 12 The comparison of the quadratic efficiency curves by using the steady state, the QDT and the L-QDT method

6. Conclusion

A brand new dynamic test method for solar collectors under transient weather conditions is developed. This new dynamic test method was characterized by using the Laplace transformation technique to solve the differential governing equation. This new Laplace transformation method can be easily expanded to combine with the QDT method. The L-QDT mathematical model is an analytical non-linear equation which describes the dynamic response process of solar collector and contains the same collector parameters as the QDT model. Two experimental methods are introduced. One is the shielding test method which needs to shield and un-shield the solar collector continuously during test period. The other is the so called natural experimental method which doesn't need manual intervention. The useful data need to be selected from the recorded test raw data. The natural test method is developed based on the theory that the unstable weather condition has the similar effect of shielding and un-shielding actions for solar collectors. The method of how to select and process data and the non-linear computation strategy are then specified.

TRNSYS simulation calculations are carried out to test the L-QDT method and the shielding experimental method. The test data was created by TRNSTS under different test conditions and used to identify the collector parameters. The results are then compared with the setting values defined by TRNSYS which show that the L-QDT mathematical model and the shielding experimental method can give accurate collector parameters under 5 or 10 s acquisition time interval.

The natural experiments were carried out on 18 June and 02-04 July 2014 at the Technical University of Denmark. A flat plate solar collector equipped with the ETFE foil was tested. The collector parameters are identified by using the L-QDT model and the selected dynamic test data and then compared with the steady state and the QDT results. The results obtained from the three test methods are statistic analyzed and compared. The close results show that the L-QDT model and the natural experimental method can be used for collector dynamic testing.

The shielding and un-shielding method is a fast test method but needs manual intervention actions. The natural experimental method can be easily carried out and save workload but needs relatively longer time. The drastic changing weather is the best condition for the natural experimental method to select suitable dynamic test data.

Above all, it can be concluded that the new Laplace test method can achieve the function of evaluating solar collector by identifying accurate collector parameters under transient weather conditions. But for a complete test method, further studies are still needed on the investigation of the behavior of the method for the complete range of the acceptable testing conditions and for different collector types, in order to obtain safe conclusions regarding the repeatability, accuracy and robustness of the method.

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