Conceptual design of a thorium supplied thermal molten salt wasteburner

Schönfeldt, Troels; Klinkby, Esben Bryndt; Klenø, K.H.; Boje, Peter; Eakes, C.; Pettersen, E.E.; Løvschall-Jensen, A. E.; Jørgensen, M. D.

Publication date:
2015

Citation (APA):
Conceptual design of a thorium supplied thermal molten salt wasteburner

Troels Schönfeldt\textsuperscript{1,2}  
E. Klinkby\textsuperscript{1,2}, K. H. Klenø\textsuperscript{2}, P. Boje\textsuperscript{3}, C. Eakes\textsuperscript{2}, E. E. Pettersen\textsuperscript{1,2,4}, A. E. Løvschall-Jensen\textsuperscript{2,4}, & M. D. Jørgensen\textsuperscript{2}.

\textsuperscript{1}DTU Nutech, \textsuperscript{2}Seaborg IVS, \textsuperscript{3}DTU Diplom, \textsuperscript{4}Niels Bohr Institute
The Project

• Me: Troels Schönfeldt: PhDc - Advanced cold neutron moderators @ DTU Nutech and ESS Neutronics
• 168 hours/week. A PhD study is 37.5 hours/week (=> 77.7% spare-time)... So we started a company
• Seaborg IVS:
  – We now consist of 10 unpaid physicist, chemists and engineers
  – We focus on nuclear reactor technologies, with special focus on molten salt reactors and thorium
• Here you will be presented with our, still very preliminary, Seaborg WasteBurner, the SWaB
Kickoff

- In December 2014 we were invited to join the “Feasibility Study for the Development of a Pilot Scale Molten Salt Reactor in the UK”, by:

  - The SWaB design - a single salt thermal molten salt wasteburner
  - The SWaB is currently under evaluation by UK experts
  - Also, it turns out that 130.5 hours/week of spare times is not really a lot
Our constraints

1: No weapons!
- No separation of Pu/Pa from U
- Highly “denatured” U and Pu
- Decreasing weapon “quality”

2: Inherently safe
- Rely on physics
- Any active system must be redundant

3: Wasteburner
- Negative net TRU production
- Evolve towards the closed thorium fuel cycle

4: Thermal spectrum operation
- Because it has tremendous advantages
- Inefficiency of TRU burning should be compensated for by enhanced neutron economy

5: Modular (Economical):
- decrease construction/decommission cost
- Shipyard style manufacturing - mass-production

Early drawing of the “bottle"
The "product"

Reactor class:
Chemistry

S. Delpech et al., Reactor physic and reprocessing scheme for innovative molten salt reactor system. Journal of fluorine chemistry, 2009
Method

- Reactor model
- Initial fuel from LWR
- Rebalance 78LiF-22AcF₄ and volume
- Time-evolve SNF
- McNPX (Cinder)
- Degasser
- Chemistry
- Refueler

Processes:
- Material
- Neutronics
- Spectrum
- Simi-automatic optimization

DTU Nutech
Center for Nuclear Technologies
Initial fuel and alternatives

Flame reactor:
SNF -> Fluoride salts and removes:
- 99.1% U (as UF₆)
- 0.1% other Ac
- 99% FP (extracted)

Initial fuel (10 year storage):
45% U (~1.3% enriched)
45% Pu (~68% fissile)
5% FP (only non-gasses)
5% minor Ac (mainly Am)
Salt and moderator

- Iterative optimization of geometry and spent fuel to Th ratio \((\text{Ac} \Rightarrow x\text{Th} + y\text{Ac}_{\text{SNF}})\) optimized to \(K_{\text{eff}}\max \sim 1.05\)
- Using this tool, we were able to analyze several moderator and carrier salt candidates in a matter of days.
Control

1: Huge “instant” negative response, mainly from salt density change.
2: Small “slow” positive response from graphite heating. (Problematic)

Daily control using online chemistry. Hourly control using 4 graphite fine-tuning rods ($\Delta$keff=0.88=$254$ pcm)
Absorbing control rods for full shutdown only (= better neutron economy)
Pot outer dimension: 190x190x340 cm³
Blanket thickness: 15-22 cm
Moderator: **Graphite** (r=75 cm, l=300 cm)
Operation temperature **700°C-900°C**
Flow speed: 38.1 l/s
Salt volume: ~6 m³ (~5 m³ in core)
Salt composition: 78LiF-22AcF₄ (99.95% ⁷Li)
  - 100Ac ~ 87Th+6U+6Pu+1Acₘ (starting)
  - Melting point <568°C
  - Salt evaporation starts: >1300°C
Running the cycle with our (thermal-epithermal) spectrum utilizes **83.1%** of the fuel and produce **16.9%** americium waste – but **eta=0.88** (sustainable is eta>>1)
Running the cycle with our (thermal-epithermal) spectrum utilizes virtually all the fuel and produce **4.56 ppm** americium waste and \( \text{eta} = 1.06 \) – however...
Neutron loss

The changing leakage over time, is caused by significant inventory changes from “over-fueling” (and Th removal) to keep the core critical.

Our thorium cycle has \( \eta = 1.06 \)

But we lose 10-13% neutrons.

<table>
<thead>
<tr>
<th>Actinide component</th>
<th>Initial</th>
<th>30 years</th>
<th>60 years</th>
</tr>
</thead>
<tbody>
<tr>
<td>Thorium</td>
<td>86.7%</td>
<td>59.6%</td>
<td>39.9%</td>
</tr>
<tr>
<td>Uranium</td>
<td>6.3%</td>
<td>21%</td>
<td>32%</td>
</tr>
<tr>
<td>Plutonium</td>
<td>6.3%</td>
<td>16%</td>
<td>23%</td>
</tr>
<tr>
<td>Minor Ac</td>
<td>0.6%</td>
<td>3.0%</td>
<td>4.8%</td>
</tr>
<tr>
<td>Fissile Pu/Pu</td>
<td>67.8%</td>
<td>53.1%</td>
<td>48.5%</td>
</tr>
</tbody>
</table>
Fissile Material

60 years, at 50 MW$_{th}$:
Net negative transuranic production of ~1 ton!
We do not have an underlying closed thorium fuel cycle.
But with the production of $^{233}$U we are getting closer.
Next step: SWaB -> CUBE
Seaborg WasteBurner -> Compact Used fuel BurnEr

Fix reactivity feedback from graphite expansion
- graphite slabs instead of salt pipes

Increase fine-tuning rods reactivity span
- move rods to a more central position

Reduce Pu (and Ac₃m) inventory
- minimize salt volume (double blanket?)
- optimize moderator configuration
- remove Am online
- increase UF6 evaporation in fuel processing

Increase neutron economy
- reduce leakage (ultra compact)
- add outer reflector

Funding needed for two activities:
System engineering and multi physics
Chemistry system design and verification

DTU Nutech
Center for Nuclear Technologies