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38.2-Gb/s Optical-Wireless Transmission in 75-110 GHz Based on Electrical OFDM with Optical Comb Expansion

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Abstract: We demonstrate scalable optical comb- and heterodyning-based generation, optical and 1.36m wireless transmission, and electrical heterodyne detection of multiband OFDM up to 38.2 Gb/s occupying 14.4 GHz RF bandwidth, for high-capacity optical-wireless links in 75-110 GHz.

OCIS codes: (060.2330) Fiber optics communications; (060.5625) Radio frequency photonics

1. Introduction

Millimeter-wave systems are a potential solution for future seamless integrated optical/wireless access as well as for mobile backhauling [1]. Millimeter-wave bands at around 60 GHz and higher could provide bandwidth enough to easily support multi-gigabit capacities. The 60-GHz band has been widely studied as it provides about 7-GHz bandwidth for unlicensed communications [1,2]. Bands of around 100 GHz and higher show larger potential bandwidths available to support very high capacities envisioned (towards 100 Gb/s) [3]. In particular, the 75-110 GHz band (W-band) can extend outdoor transmission distances due to its lower atmospheric loss. Radio-over-fiber systems in the 75-110 GHz band are recently attracting more and more interest to deliver 40 Gb/s and beyond [1, 4-7]. Wireless transmission systems in the 75-110 GHz band have been reported up to 20 Gb/s [4] based on ASK data modulation. Spectral efficient modulation formats have also been employed, up to 3 cm of wireless distance at 20 Gb/s based on QPSK [5] or at 40 Gb/s based on 16-QAM [6]. A system based on optical OFDM with optical down-conversion has also been demonstrated without wireless transmission [7].

In this paper, we report on the optical generation, combined optical and 1.3-m wireless transmission, and electrical detection in the 75-110 GHz band of electrical OFDM based on 16-QAM subcarrier modulation up to 38.16 Gb/s occupying 14.4 GHz RF bandwidth, for high-capacity optical-wireless links in 75-110 GHz.

2. Experimental setup

Figure 1 shows the schematic of the experimental setup. At the optical OFDM transmitter, a baseband OFDM signal is generated by offline digital signal processing (DSP), which is then stored in an arbitrary waveform generator (Tektronix AWG7122C). In the offline DSP, a data stream consisting of a pseudo-random bit sequence (PRBS) of length $2^{15}-1$ is mapped onto 72 16-QAM subcarriers, which, together with 8 pilot subcarriers, one zero-power DC subcarrier, and 47 zero-power edge subcarriers, are converted to the time domain via an IFFT of size 128. A cyclic prefix of length 13 samples is employed, resulting in an OFDM symbol size of 141. To facilitate OFDM frame synchronization and channel estimation, 10 training symbols are inserted at the beginning of each OFDM frame that contains 150 data symbols. The real and imaginary parts of the OFDM signal are clipped and converted to analog signals by two D/A converters operating at 5 GS/s with a D/A resolution of 10 bits. The two analog signals from the AWG are filtered by two antialiasing low-pass filters (LPF) with 2.5-GHz bandwidth. The two filtered signals are amplified and applied to an optical I/Q modulator, which is biased at the minimum transmission point, connected to an external-cavity laser (ECL, $\lambda = 1550.6 nm$) with 100-kHz linewidth. An optical OFDM signal at 9.57 Gb/s (5 Gb/s×72/141×150/160) with a bandwidth of 3.164 GHz (5 GHz×81/128) is thus generated. An Erbium-doped fiber amplifier (EDFA) is employed to compensate for loss and an optical band-pass filter with 0.8-nm bandwidth is employed to filter out-of-band noise. Subsequently, the optical OFDM signal is expanded by a comb generator based on an overdriven phase modulator (PM) [8] to form a five-band 47.85-Gb/s signal. The generated comb is
filtered by a 25-GHz fiber Bragg grating (FBG) filter operating in reflection, as shown in Fig. 2(a), to reduce crosstalk penalty. The frequency spacing of the comb lines is set to 3.75 GHz to minimize crosstalk penalty while maximizing spectral efficiency. After EDFA amplification and noise filtering, the optical five-band OFDM signal at point (1) in Fig. 1 is amplified and combined with an unmodulated CW optical carrier (ECL, $\lambda = 1549.9\text{nm}$) with 100-kHz linewidth. The combined optical five-band OFDM signal and the unmodulated CW carrier would be transmitted to a remote antenna site where they are heterodyne mixed in a 100-GHz photodetector (u't XPDV4120R). Optical transmission over 22.8 km of standard single-mode fiber (SSMF) is evaluated in the experiment. The signal after photodetection is the electrical OFDM signal at the desired RF carrier frequency, which is fed to a rectangular horn antenna in the 75-110 GHz band with 24-dBi gain. Fig. 2(b) shows the spectrum of the combined optical signal at point (2) in Fig. 1, the RF carrier frequency is set to 88 GHz. After wireless transmission, the RF OFDM signal is received by another rectangular horn antenna in the 75-110 GHz band with 25-dBi gain. The received signal is amplified by a low-noise amplifier (LNA, Radiometer Physics 75-105 GHz) with 25-dB gain. Frequency down-conversion of the RF OFDM signal is performed by electrical mixing (75-110 GHz RF, 1-36 GHz IF) with a local oscillator (LO) signal at 74 GHz. The LO signal is generated by frequency doubling a 37-GHz signal from a signal generator (Rohde&Schwarz SMF100A). The down-converted signal is sampled at 80 GS/s by a digital signal analyzer with 32-GHz real-time bandwidth (Agilent DSA93204A) and demodulated by offline DSP. The receiver-side DSP blocks are shown in Fig. 1. In the receiver DSP, first, frequency down-conversion and LPF is performed to extract each baseband OFDM band. For each baseband OFDM band, synchronization, frequency and channel estimation, pilot-assisted phase estimation, data recovery by symbol mapping and serialization, and bit error rate (BER) test is performed. To eliminate the dispersion and nonlinearity effects induced by fiber and wireless transmission, one-tap equalizer and an effective algorithm combining intra-symbol frequency-domain averaging [9] and digital phase-locked loop are used for channel estimation. BER is evaluated by counting the number of errors considering 42912 bits.

3. Experimental results

Up to 4 RF OFDM bands out of the 5 optical OFDM bands can be demodulated within the FEC limits due to the frequency response of the photodetector. Fig. 3 shows the electrical spectra of the single-band and four-band OFDM signals after sampling at the receiver. BER performance of the four-band OFDM signal at 38.16 Gb/s has been evaluated and compared with the performance of the 9.57-Gb/s single-band OFDM signal without comb expansion, i.e. when the RF signal driving the PM is off. Examples of recovered constellations are also shown in Fig. 3. Fig. 4 shows the measured BER as a function of the received optical power at point (3) in Fig. 1. Fig. 4(a) shows BER for combined optical and wireless transmission of the single-band OFDM signal. The receiver sensitivity at the FEC
OFDM signal (3.26GHz RF bandwidth) has been transmitted over 22.8 km of SSMF and a comb expanded OFDM supporting future high capacity hybrid optical-wireless applications approaching 50 Gb/s and beyond. A 9.66Gb/s transmission with a BER performance within FEC limits, showing the potential of multiband electrical OFDM.

4. Conclusion

We have demonstrated bandwidth scalability, up to five sub-bands, of electrical 16QAM-OFDM signals in the 75-110 GHz band employing optical comb generation. We have demonstrated optical and up to 1.3 m wireless transmission with a BER performance within FEC limits, showing the potential of multiband electrical OFDM in supporting future high-capacity hybrid optical-wireless applications approaching 50 Gb/s and beyond. A 9.6-Gb/s OFDM signal (3.2-GHz RF bandwidth) has been transmitted over 22.8 km of SSMF and a comb-expanded OFDM signal up to 38.2 Gb/s (14.4-GHz RF bandwidth) has been demonstrated for short-distance applications.

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6. References