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Second harmonic imaging using synthetic aperture sequential beamforming

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Abstract—The paper investigates Second Harmonic Imaging (SHI) using Synthetic Aperture Sequential Beamforming (SASB). The investigation is made by an experimental Synthetic Aperture Real-time Ultrasound System (SARUS). A linear array transducer is used to scan 4 wires at the image depths of {22.5, 47.5, 72.5, 97.5} mm, respectively. Three different experiments are made using three different transmit foci at 10 mm, 25 mm and 50 mm. A 2-cycle sine wave with a center frequency of 5 MHz is used as the excitation. The SHI is achieved by using Pulse Inversion (PI) technique. The data received with and without PI from SARUS are beamformed using Dynamic Receive Focusing (DRF) and SASB by a Beamformation Toolbox. The Full Widths at Half Maximum (FWHM) in both the lateral and axial directions for these four wire targets using different imaging algorithms (DRF, DRF+SHI, SASB and SASB+SHI) are calculated and shown in the paper. The Full Width at One Tenth Maximum (FWOTM) is also investigated. By combining SASB and SHI, the lateral resolution is improved by 66%, 35% and 46% for FWHM, and 52%, 20% and 29% for FWOTM, compared to DRF, DRF+SHI and SASB, respectively. The axial resolution is improved 24% on average by SHI.

I. INTRODUCTION
Non-linear ultrasound may be combined with different imaging methods to further improve the resolution. The conventional harmonic imaging uses a fixed transmit focus and dynamic receive focus (DRF). Synthetic aperture imaging is a well-know ultrasound imaging method, where dynamic focusing can be achieved in both transmit and receive. Synthetic aperture harmonic imaging has been introduced by Bae et al [1] in 2008. In conventional synthetic aperture imaging, a single element is used for emissions to simulate a spherical wave. The major drawback is that the transmitting energy for a single element is too low, so that the harmonic signals are very weak. Although there can be a multi-element emission used to enhance the transmitting energy and simulate a virtual focal point behind or in front of the transducer, it still requires a lot of memory for saving the data for each low resolution image, when using the conventional synthetic aperture imaging.

Synthetic aperture sequential beamforming (SASB) is a novel technique, also called dual-stage beamforming, which has been researched and developed by Kortbek et al [2], [3] in 2007. The advantage of SASB is that the lateral resolution is improved independently of image depth compared to the conventional ultrasound imaging using DRF. SASB can be thought of as a two-stage procedure. The first stage is to obtain a set of conventional B-mode image lines with a fixed transmit and receive focal point. Then the image is created by synthetic aperture imaging using the B-mode image lines in the second stage. In this way, not only is dynamic focusing in both transmit and receive achieved, but the memory requirement is also reduced, since each low resolution image is only stored in one B-mode image line. In the first stage of SASB, a number of elements are used for a fixed focus transmission. Thus, a high penetration depth and SNR for harmonic imaging can be attained.

The purpose of this study is to investigate harmonic imaging using the dual-stage synthetic aperture sequential beamforming. The measured results using different imaging methods are illustrated and compared in the following sections. A discussion based on the measured results and a final conclusion are given at the end of the paper.

II. METHOD
The measurement setup is illustrated in Fig. 1. The investigation is made by an experimental scanner - Synthetic Aperture Real-time Ultrasound System (SARUS) [4]. A linear array transducer (BK8804, from BK Medical Aps) is used to transmit and receive data from a wire phantom in water. Four wires are used as point targets at the image depths of 22.5 mm, 47.5 mm, 72.5 mm and 97.5 mm, respectively. Three different experiments are made using three different transmit...
foci, which are 10 mm, 25 mm and 50 mm from the transducer surface. A two-cycle sine wave with a center frequency of 5 MHz is used as the excitation.

Four imaging methods are investigated: dynamic receive focused imaging (DRFI), dynamic receive focused second harmonic imaging (DRFSHI), synthetic aperture sequential beamformed imaging (SASBI), and synthetic aperture sequential beamformed second harmonic imaging (SASBSHI). The second harmonic imaging is achieved using a pulse inversion technique [5], [6]. This is made by using two excitations with a 180° phase difference, sending them in turn for each emission and summing the two received RF lines. The odd harmonic components (1st(fundamental), 3th, 5th, etc.) are canceled out during this process. Then a matched filter is applied to remove the higher even harmonic components (4th, 6th, 8th, etc.) and leave the second harmonic component only. The received RF lines obtained from SARUS after pulse inversion are post-processed by a Beamformation Toolbox [7], [8] to achieve the DRF and SASB.

Fig. 3: Lateral FWHM for 4 points along depth - TF10, TF25 and TF50 denote transmit foci are at 10 mm, 25 mm and 50 mm.

Fig. 4: Lateral FWOTM for 4 points along depth - TF10, TF25 and TF50 denote transmit foci are at 10 mm, 25 mm and 50 mm.

III. RESULTS

The images for the wire phantom using the different methods are shown in Fig. 2. The FWHM (full width at half maximum (at -6 dB)) and FWOTM (full width at one tenth maximum (at -20 dB)) along the lateral direction are calculated for each point with different methods and transmit foci, and plotted in Figs. 3 and 4. The comparison among these 4 imaging methods should be made using the best possible setup for each method. Three measurements with different transmit foci were made for each method. The FWHM and FWOTM for these 4 measured points and the average resolution as a function of depth are evaluated for different transmit foci in each method. After the evaluation, the "best" image with an optimized transmit foci is used to compare with the other imaging methods. The optimization is performed by comparing the FWHM and FWOTM for each point. The shortest FWHM and FWOTM will get 1 point, and no point for others, so that there will be eight (4 for FWHM and 4 for FWOTM) comparisons among 3 transmit foci. The total score will be divided by its average FWHM in millimeter. The final scores are shown in Table I.

Hereby, the final comparison between the different imaging methods is made among DRFI (TF: 50 mm), DRFSHI (TF: 50 mm), SASBI (TF: 10 mm) and SASBSHI (TF: 10 mm) as show in Fig. 5. By calculating the average FWHM and FWOTM for those four points, the lateral resolution of SASBSHI is improved by 66%, 35% and 46% for FWHM, and 52%, 20% and 29% for FWOTM compared to DRFI, DRFSHI and SASBI, respectively.

To show the axial resolution, the center image lines, which go through the point target, are plotted for each method for the second wire (P2) as shown in Fig. 6. The envelopes of the pulses using these four methods DRFI, DRFSHI, SASBI and SASBSHI are plotted in Fig. 7a. The received pulse length becomes shorter for harmonic imaging. However, SASBI does not reduce the length of the pulse compared to DRFI. The results for the FWHM in the axial direction using different imaging methods can be found in Fig. 7b. The axial FWHM of SASBSHI is improved by 27%, 5% and 25% compared to DRFI, DRFSHI and SASBI, respectively.
IV. DISCUSSION

Fig. 5a shows that the SASBSHI gives a minimum FWHM in terms of the image resolution and it maintains the same values along the depth. However, it can be found that the FWOTM using SASBSHI is increased as a function of depth as shown in Fig. 5b. This is because that the harmonic signals are weak at the depth far from the transducer, since the transmit foci is 10 mm for the SASB. The noise will have much stronger impact on the harmonic signals at -20 dB than that at -6 dB. The previous study of SASB by Kortbek [2] showed that the transmit foci was preferred to be close to the transducer surface to get a better resolution from the SASB. The combination of SASB and SHI is supposed to meet the compromise that the harmonic signals are not reduced too much in the deep depth, meanwhile the transmit foci is still close enough to the transducer to ensure SASB functioning. This can be optimized by doing parameter studies in the future work by trying more different transmit focal distances at the first stage of SASB. The resolution can be investigated by calculating the full width at -20 dB and -40 dB as a function of image depth. Fig. 7b indicates that the axial FWHM using SHI (green and red lines) is lower than that without using SHI (blue and black lines) and there is no much decrease for the axial FWHM no matter whether the SASB is used or not (black line compared to blue line, or red line compared to green line).

V. CONCLUSION

In this study wire phantom measurements were made by a research scanner SARUS using 7 MHz BK8804 linear array transducer. Four different imaging algorithms (DRFI, DRFSHI, SASBI and SASBSHI) were investigated using three different transmitting foci (10 mm, 25 mm and 50 mm from the transducer surface). SASBSHI improved the lateral resolution by 66%, 35% and 46% for FWHM (-6 dB), and 52%, 20% and 29% for FWOTM (-20 dB), compared to DRFI, DRFSHI, and SASBI, respectively. The axial resolution was improved by 24% using SHI.
Fig. 5: Lateral full width at -6 dB (FWHM - top figure) and -20 dB (FWOTM - bottom figure) - The transmit foci for the DRFI and DRFSHI is 50 mm and for the SASBI and SASBSHI it is 10 mm. The 4 wires are at depths of 22.5 mm, 47.5 mm, 72.5 mm and 97.5 mm.

Fig. 6: Pulses and envelopes in the axial direction using different imaging methods - These show the center image lines for DRFI, DRFSHI, SASBI, SASBSHI and their envelopes. The second point target (P2) along the scanning depth and is around 47.5 mm from the transducer surface. The transmit foci is 50 mm for DRFI and DRFSHI, and it is 10 mm for SASBI and SASBSHI.

Fig. 7: Envelops and axial FWHM - The envelopes for DRFI, DRFSHI, SASBI and SASBSHI are plotted together in the top figure. The values of the axial FWHM for each method are shown in the bottom figure.

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