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EFFECT OF EQUAL CHANNEL ANGULAR EXTRUSION ON CORROSION BEHAVIOUR OF Al-Mn ALLOY

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The formation of a highly deformed layer at the surface of rolled aluminium alloy sheet results from shear deformation during rolling. Subsequent annealing leads to enhanced precipitation of fine intermetallic particles in the surface layers. (1-3) These layers have high electrochemical reactivity, in particular, a strong susceptibility to filiform corrosion. (2, 4-5) This deformed layer also has a detrimental effect on other types of localised corrosion. (6-8)

In order to understand the role of deformation on corrosion behaviour of Al-Mn alloy, an Al-1Mn-0.4Fe-0.3Si model alloy was deformed by Equal channel angular extrusion (ECAE) and followed by annealing. The die angle for the extrusion was $\phi = 120^\circ$. The rods were pressed with a ram speed 40 mm/min at room temperature. The cycle was repeated each time without any rotation between passes. Samples were pressed 3, 10 and 15 times. It was found that deformation by ECAE followed by annealing leads to an increase in the number and % area of intermetallic particles. The manganese content in the matrix of the alloy after deformation during rolling. Subsequent annealing leads to enhanced precipitation of fine intermetallic particles in the surface layers. (1-3) These layers have high electrochemical reactivity, in particular, a strong susceptibility to filiform corrosion. (2, 4-5) This deformed layer also has a detrimental effect on other types of localised corrosion. (6-8)

In order to understand the role of deformation on corrosion behaviour of Al-Mn alloy, an Al-1Mn-0.4Fe-0.3Si model alloy was deformed by Equal channel angular extrusion (ECAE) and followed by annealing. The die angle for the extrusion was $\phi = 120^\circ$. The rods were pressed with a ram speed 40 mm/min at room temperature. The cycle was repeated each time without any rotation between passes. Samples were pressed 3, 10 and 15 times. It was found that deformation by ECAE followed by annealing leads to an increase in the number and % area of intermetallic particles. The manganese content in the matrix of the alloy after different levels of ECAE processing and heat treatment was determined using thermoelectric power (TEP) measurements. The higher number of ECAE passes result in the %Mn in solid solution decreasing as shown in Fig. 1.

Electrochemical measurements were carried out in 0.1 M NaCl. ECAE deformed samples have a higher cathodic reactivity than the undeformed sample as shown in Fig. 2. Furthermore, the higher levels of deformation increased the cathodic reactivity resulting from the breakdown of intermetallic particles into smaller particles when deformed and precipitated more intermetallic particles on the surface after heat-treatment. The anodic polarisation measurements were conducted in 0.1 M NaCl, pH 11.5. The passive current density was $10^{-7}$ to $10^{-5}$ A/cm$^2$. The ECAE 15 passes and subsequently annealed sample was more anodically active than the undeformed and annealed sample.
The corroded surfaces after anodic polarisation showed the localised corrosion (pitting) sites on the surface. The number of pitting sites on the undeformed sample is less than that on the deformed sample. These are related to the number of intermetallic particles on the surface. It has been suggested that the increased precipitation on the deformed samples causes a decrease in solute content (Mn) of the matrix, thus enhancing the anodic reactivity.

References

Fig. 1. %Mn in solid solution of the undeformed and ECAE-deformed Al-1Mn-0.4Fe-0.3Si alloy.

Fig. 2. Cathodic polarisation of Al-1Mn-0.4Fe-0.3Si with different numbers of ECAE passes and subsequent annealing in naturally 0.1 M NaCl.

Fig. 3. Anodic polarisation of Al-1Mn-0.4Fe-0.3Si in naturally aerated 0.1 M NaCl, pH 11.5.

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