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Towards Ultrahigh Speed Impulse Radio THz Wireless Communications

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ABSTRACT

THz impulse radio technologies promise a new paradigm of fast wireless access with simplified wireless reception. However, huge loss of propagating broad bandwidth THz impulse radio signals limits THz wireless transmission distance and reduces the achievable link data rates. In this paper, we evaluate the realistic throughput and accessible wireless range of a THz impulse radio communication link based on a uni-travelling photodiode (UTC-PD) as THz emitter and a photoconductive antenna (PCA) as THz receiver. The impact of highly frequency-selective THz channel and the noise in the system are also considered.

Keywords: THz photonics, THz wireless communication, impulse radio, photoconductive sampling.

1. INTRODUCTION

THz technologies have been widely recognized as next frontier for developing ultrafast wireless communication [1][2], aiming at accommodating up to Terabit-per-second (Tbps) wireless data rates in 2020. The most challenging aspects are obviously the development of efficient ultra-broadband components operating in the THz frequency bands, particularly for generating and detecting THz communication signals. Up to date, a lot of efforts have been put on developing the photonic devices, utilizing the extremely fast photoresponse and hence overcoming the bandwidth limitation in the electronic techniques. More specifically, uni-travelling carrier photodiodes (UTC-PDs) have been of great interest in opto-electronic generation of THz signals due to the very large bandwidth and high THz conversion efficiency [3]. The most recently developed UTC-PD has exhibited a bandwidth up to 2.5 THz [4].

From the viewpoint of a communication system, the impressive performance of the UTC-PDs accelerates the development of high speed photonic wireless communications. The UTC-PDs have indeed been widely used in the demonstrated millimeter-wave and sub-THz wireless systems [5]-[17]. Figure 1 summarizes recent contributions on progressing high speed photonic wireless communication systems, in the frequency range of 100 GHz – 600 GHz [7]-[17]. These systems operate in different narrow frequency windows, and thus suffer less loss from the atmospheric propagation. However, there is only tens of GHz bandwidth available for each single frequency window, which makes narrow band carrier modulation technique difficult to approach Tbps, as minimum 200 GHz bandwidth will be required to obtain a reasonable signal-to-noise ratio for a Tbps signal. To further increase the throughput of a THz communication system, most attentions are so far paid to apply multidimensional modulation schemes (amplitude modulation, phase modulation, frequency multiplexing, time multiplexing and polarization multiplexing). It noted the increasing of THz spectral efficiency requires higher linearity and larger spur free dynamic range.

Figure 1. Reported high speed sub-THz/THz carrier modulation communication systems.

Alternatively, a THz impulse radio (IR) communication, similar to impulse radio ultra-wideband systems (3.1 – 10.6 GHz) [18][19], has also the potential of supporting very large capacity at a scale of Tbps within a small wireless coverage (<1 m) [20][21], by exploring an extremely large RF frequency band for communication. In addition, a pulsed system features some other advantages, e.g. larger bandwidth (simple modulation scheme), easily recoverable distortion and less noise effect. At the receiver side, low-temperature-
grown GaAs photoconductive antennas (PCAs) can be an option, as they typically consume sub-nJ energy per pulse and can handle sufficiently large bandwidth in the UTC-PD. The capacity of a THz impulse radio communication link has been theoretically analyzed in [20], but the realistically achievable link throughput relies on the performance of THz components employed and reception scheme, and this is not yet investigated.

In this paper, we will estimate the realistic throughput and accessible wireless range of a THz impulse radio wireless communication link by employing a UTC-PD as THz emitter and a photoconductive antenna as THz receiver. The link performance will be reasonably analyzed by taking into account the impact of THz frequency-selective channel properties and the noise in the system.

2. THz IMPULSE RADIO SYSTEMS AND PERFORMANCE ANALYSIS

2.1 THz impulse radio systems

The schematic THz impulse radio communication system under consideration in this paper is shown in Fig. 2. A time-multiplexed ultrashort optical pulse train at very high data rates well beyond 100 Gbps is launched into a THz emitter. The illumination of each optical ultrashort pulse at the emitter correspondingly generates a THz pulse, and then radiated by an antenna integrated in the THz emitter. After free space transmission, the THz pulse train is wirelessly received by a THz receiver. In order to release bandwidth requirements in receiving such an ultrahigh speed signal, we will consider time demultiplexing technique in the receiver. A sampling pulsed laser at a relatively low repetition rate (e.g. 10 GHz) is used to demultiplex ultrafast THz pulse train into the base rate of sampling laser. In our system, we will consider an ultra-broadband UTC-PD and a PCA as the THz emitter and receiver, respectively. Both of these two components are commercially available and commonly used in THz systems.

![Figure 2. Concept of an ultrafast THz impulse radio communication link employing optical time multiplexing at the transmitter and time demultiplexing at the receiver. THz emitter: UTC-PD, THz receiver: PCA.](image)

2.2 Noise in the system

There are several major noise sources in the THz communication system above, and molecular absorption noise in the wireless channel and thermal noise/shot noise in the UTC-PD are dominant, amongst others. When the molecular absorption is considerably high in the system, the internal vibration of the molecules turns into the emission of THz radiation at the same frequency that the incident waves that provoked this motion, which can be considered as a noise factor [20] and estimated by

\[
\sigma_{mol}^2(f, d) = k_B T \int_0^\infty \left[ 1 - e^{k(f)d} \right] df
\]

where \( k(f) \) denotes the absorption strength, the absorption coefficient at the frequency component \( f \), \( d \) is wireless distance, \( T \) is the operating environment temperature of the system, \( k_B \) is the Boltzmann constant, and \( B \) is the effective noise bandwidth.

The shot noise is dependent on the average photocurrent \( I_{avg} \) in the photodiode and the thermal noise does not.

\[
\sigma_{shot}^2 = 2qRP_{avg}B
\]

\[
\sigma_{thermal}^2 = 4k_B T/R_l \cdot B
\]

Here \( q \) is the electron charge, \( R \) is the responsivity of the UTC-PD, \( P_{avg} \) is the average optical power and \( R_l \) is the load resistor. The total noise in the system will be

\[
\sigma_{total}^2 = \sigma_{mol}^2 + \sigma_{shot}^2 + \sigma_{thermal}^2
\]

2.3 Performance analysis

In our numerical analysis, a commercially available UTC-PD with a 3 dB bandwidth of 310 GHz and a DC responsivity of 0.25 A/W is considered. The system performance is estimated by analyzing the performance of demultiplexed 10 GHz signals after free space wireless propagation, in terms of wireless distance-dependent signal to noise ratio and Q factor. The wireless propagation is considered in an office- or lab-based indoor environment (20°C and 51% relative humidity). The PCA considered here features very fast photoresponse...
which is governed by its trapping time (0.7 fs) and trap emptying time (10 fs). The average power launching into the UTC-PD and the PCA are respected to be below their thermal damage thresholds, and they are 20 mW for the THz emitter and 30 mW for the THz receiver, respectively. The strength of the absorption by a specific type of molecules is directly obtained from the Jet Propulsion Laboratory (JPL) database.

Figure 3(a) shows 640 Gbps THz IR signal generated from 100 fs ultrashort optical pulse train and the impact of wireless propagation on the waveform of THz pulses. We can see that each optical pulse individually generates a THz pulse. The emitted THz pulses are monocycle-like, because THz radiation in a dipole or bow-tie antenna is proportional to the derivative of the instantaneous current flowing through the antenna gap. It is noted that noise in the system is not included, but we can observe that the THz pulses after 1m wireless distance exhibits noise-like background in the time domain, which apparently degrades the received signal to noise ratio. This is because the ultrashort THz pulse is extremely broadband in the frequency domain and the wireless propagation channel is highly selective, particularly in the frequency components above 1 THz.

The quality of 640 Gbps THz impulse radio signals is evaluated by calculating Q factor of wirelessly received 10 GHz pulses. Taking into account the noise in the system, the demultiplexed 10 GHz THz pulse trains after 0.1 m wireless propagation is presented in Fig. 3(b), and the SNR in this case is 22 dB, which can be expected to achieve a Q factor of 10.6. The wireless distance dependent Q factor for demultiplexed 10 GHz signals is shown in Fig. 3(c). We can see that within the wireless range of < 0.5 m, performance of below the forward error correction (FEC, bit-error rate (BER) of 2e-3) can be achieved.

3. CONCLUSIONS
THz impulse radio technology explores extremely broadband RF frequency for communications and has a high potential of realizing ultrahigh speed wireless data rates. We have evaluated the realistic throughput and accessible wireless range of a THz impulse radio communication link based on commercially available THz components, an UTC-PD as THz emitter and a PCA as THz receiver. 640 Gbps THz impulse radio throughput can be supported in room temperature environment in a small cell range (< 0.5 m) by employing time demultiplexing scheme for receiver. The limited access range is due to huge loss and additional noise caused by the THz propagation channel. Therefore, impulse radio Tbps THz communication would find applications in nanocell backhaul, short range interconnections, superfast board-to-board communication, and some particular cases of wireless delivering large volume of data (e.g. E-healthcare images).

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REFERENCES
[4] T. Ishibashi et al.: Continuous THz wave generation by photodiodes up to 2.5THz, in Proc. IRMMW 2013, Germany.


