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Optical and electrical properties of polycrystalline and amorphous Al-Ti thin films

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The structural, optical, and transport properties of sputter-deposited Al-Ti thin films have been investigated as a function of Ti alloying with a concentration ranging from 2% to 46%. The optical reflectivity of Al-Ti films at visible and near-infrared wavelengths decreases with increasing Ti content. X-ray absorption fine structure measurements reveal that the atomic ordering around Ti atoms increases with increasing Ti content up to 20% and then decreases as a result of a transition from a polycrystalline to amorphous structure. The transport properties of the Al-Ti films are influenced by electron scattering at the grain boundaries in the case of polycrystalline films and static defects, such as antisite effects and vacancies in the case of the amorphous alloys. The combination of Ti having a real refractive index ($n$) comparable with the extinction coefficient ($k$) and Al with $n$ much smaller than $k$ allows us to explore the parameter space for the free-electron behavior in transition metal-Al alloys. The free electron model, applied for the polycrystalline Al-Ti films with Ti content up to 20%, leads to an optical reflectance at near infrared wavelengths that scales linearly with the square root of the electrical resistivity. © 2016 AIP Publishing LLC. [http://dx.doi.org/10.1063/1.4945769]

Much attention has been paid to the prediction and measurements of optical reflectivity of metallic films due to their use in a wide variety of applications ranging from solar reflectors to reflector layers on recordable or erasable-rewritable compact discs. Aluminum is an attractive material due to its high reflectivity, and tailoring its electrical resistivity can be achieved by adding metallic impurities (alloying). Alloying with transition metals (TMs), such as Ti, has turned out to diminish premature fatigue issues associated with stress, as well as enhancing the corrosion resistance and the hardness compared to pure Al.1,2 Amorphous Al-Ti alloys exhibit a higher resistance against pitting corrosion compared to the crystalline counterpart.3 In aluminum alloys containing transition metals, there will be an s-d electron scattering contribution to the residual resistivity4 which also depends upon atomic ordering of the alloys. It is thus important to investigate changes in optical reflectance of metallic alloys as a function of electrical resistivity.

The reflectance of a material can be expressed as

$$R = 1 - \frac{4n}{(n+1)^2 + k^2},$$

where $n$, $k$ are the real and imaginary parts of the refractive index, respectively. In near–infrared region when $n(\omega) \ll k(\omega)$, the reflectance can be approximated by the simple expression:

$$R \approx 1 - \frac{4n}{k^2}.$$  \hspace{1cm} (2)

Eq. (2) can be further expressed in terms of the material constants $\tau$, $\mu$, and $\rho$, where $\tau$ is the electron scattering time, $\mu$ is the magnetic permeability, and $\rho$ is the specific electrical resistivity:

$$R \approx 1 - 2\frac{\tau}{\mu} - \frac{1}{\tau} - \frac{1}{\rho^{1/2}}.$$  \hspace{1cm} (3)

The free electron model was previously used to correlate optical reflectance with electrical resistivity of multi-component sputtered alloys, such as AgMgAl5,6 and Al-Ni-Y metallic glasses.7 The aim of the paper is to investigate the role of Ti alloying on the structural, transport, and optical properties of the sputter-deposited Al thin films. The correlation between the optical reflectivity and electrical resistivity of the Al-Ti alloys will be discussed based on the Drude electron model.

The Al-Ti alloy thin films were deposited by DC magnetron sputtering using two high purity targets of Al (99.99%) and Ti (99.99%). The film composition was varied by changing the relative power on the Al and Ti targets. The Ar pressure during deposition was 185 mPa. The distance between the targets and sample was about 100 mm, and the bias voltage on the substrate was fixed at −60 V. The substrate temperature during deposition was between 70 and 100 °C. The composition of the films was determined by Rutherford Backscattering Spectrometry (RBS) and Energy Dispersive X-ray Spectroscopy (EDX), and the thickness of the films was measured by profilometry. The crystal structure was determined by grazing incidence X-ray diffraction (GI-XRD). The sheet resistance ($R_s$) was measured by a four-point probe system, and the electrical resistivity $\rho$ was subsequently calculated as $R_s \times d$, where $d$ is the film thickness. The total reflectivity was measured with an integrating sphere system over the wavelength range from 400 to 990 nm. A detailed description of the setup is given elsewhere.8 The local structure around Ti atoms was investigated by Extended X-ray Absorption
Fine Structure (EXAFS) spectroscopy at Ti K-edge (~4966 eV) at the microXAS beamline, Swiss Light Source, Switzerland. The spectra were recorded at room temperature, using an X-ray beam size of $1.0 \times 0.6 \text{ mm}^2$, delivered by the Si(111) monochromator crystals with an energy resolution of ~0.3 eV. The samples have been measured in fluorescence mode, with a single-element solid state detector (from Ketek) with 180 eV energy resolution. The X-ray absorption data were analyzed following standard procedures using the Demeter software package.9

X-ray diffraction (XRD) patterns of representative sputter-deposited Al-Ti thin films with Ti content ranging from 2% to 46% are shown in Fig. 1. All films have a thickness of about 110 ± 20 nm. For the films with a Ti content varying from 2% to 15%, only the Al fcc phase is observed, with intense reflections along the (111) and (200) directions indicating a polycrystalline structure. The solubility of Ti in Al is about 1.3% in thermal equilibrium.10 The detection of a single Al fcc phase suggests that Ti atoms occupy regular positions in the Al fcc lattice. The XRD diffraction peaks broaden with increasing Ti content suggesting a decrease of the grain size. Indeed, the grain size estimated from the full width at half maximum of the (111) reflection of the Al fcc phase is 33, 27, and 17 nm for Al-Ti films with Ti content of 2%, 5%, and 15%, respectively. The data indicate that Ti acts as an efficient grain refiner in the Al alloys, which is in agreement with previous findings.11,12 For the Al$_{50}$Ti$_{20}$ film, the intensity of the peaks increases significantly again and shifts to higher 2$\theta$ values, while the grain size is estimated to be around 27 nm. The shift cannot be associated with the formation of the Al$_{1}$Ti$_{2}$ phase typically observed at higher 2$\theta$ values. The crystal structure is probably associated with the formation of an ordered Al$_{1-x}$Ti$_{x}$ metastable phase. Films with Ti content of 24% and above have broad diffraction peaks characteristic of an amorphous structure. Our data are consistent with previous findings of thin films of sputter-deposited Al-Ti alloys to become amorphous at large Ti concentrations.13 EXAFS spectroscopy at the Ti K-edge was used to investigate the local structure around the Ti atoms. The experimental data in Fig. 2 (shown with points) that aligned with the model (shown with lines) involved analysis of the first Ti-Al shell situated at 2.69 Å in the fcc crystal structure. The Fourier transformed (FT) EXAFS spectra are shown in Figs. 2(a) and 2(b), and the derived structural parameters, such as the coordination number (NN), distance to the nearest neighbors (R), and Debye Waller factor $\sigma_0^2$ (which includes a static disorder and thermal vibrations), are given in Table I. As observed in Fig. 2(a), the amplitude of the FT peak corresponding to the polycrystalline alloys (Al$_{1-x}$Ti$_{x}$, x up to 20%) increases with increasing Ti content and reaches a maximum for Al$_{80}$Ti$_{20}$ (Fig. 2(a)). Consequently, the Debye Waller factor decreases suggesting an increase of the structural ordering around Ti atoms. The lowest $\sigma_0^2$ value was obtained for the Al$_{50}$Ti$_{20}$ film which indicates a highly ordered phase. In contrast, the amplitude of the peak corresponding to the amorphous alloys (Al$_{1-x}$Ti$_{x}$, x of 25% and above) drops significantly compared to the crystalline counterpart (Fig. 2(b)). The $\sigma_0^2$ values are larger compared to the crystalline alloys, while the NN is significantly reduced, suggesting that the disorder around Ti atoms is significantly higher compared to the crystalline counterpart. Amorphous alloys have a lower coordination number and smaller average inter-atomic distance compared to the crystalline counterpart, and this trend is more pronounced for Al$_{46}$Ti$_{54}$ and Al$_{54}$Ti$_{46}$ (see Table I). The trend can result from an increased sp-d hybridization,16 perhaps as a
The electrical resistivity of the Al-Ti films increases with Ti content, as shown in Fig. 3. In Aluminium alloyed with transition metals, there will also be an sp-d electron scattering contribution to the resistivity. Polycrystalline Al-Ti films of a single fcc structure (Ti content up to 15%) consist of nanoscale grains that decrease in size with increasing Ti content. Consequently, the electrical resistivity increases as a result of enhanced electron scattering at the grain boundaries. For a Ti content of 20% and above, the electrical resistivity of the films is larger than $100 \mu\Omega \times \text{cm}$. The origin of the high resistivity of the Al$_{80}$Ti$_{20}$ ordered phase needs to be further studied. Mooij et al. have indicated that in materials with high electrical resistivity ($>100 \mu\Omega \times \text{cm}$), the mean free path of the conduction electrons is of the order of the short range order of the materials. The large electrical resistivity values of the amorphous films can probably be associated with scattering of conduction electrons by 3d-Ti metal ions at Al-site and vacancies ($V_{\text{Ti}}$ or $V_{\text{Al}}$) rather than microscopic defects, such as grain boundaries.

The optical reflectance spectra of Al$_{1-x}$Ti$_x$ alloys at visible and near infrared wavelengths are shown in Fig. 4. Upon alloying, optical reflectance decreases gradually with increasing Ti content, both at visible and near infrared wavelengths. Pure Al has a high reflectance in the visible and near infrared spectral range and exhibits a reflectivity drop at around 800 nm due to intraband transitions, as shown in the inset in Fig. 4. Low Ti alloying (2 and 5 at. % Ti) results in a significant weakening of the intraband transitions and shift of the position of the peak towards higher photon energy. For Ti content of 10 at. % and above, the reflectance spectra decrease significantly and the absorption peak associated with the intraband absorption vanishes. The disappearance of the absorption dip for Ti content above 10% indicates that the band structure of Al is significantly affected by Ti 3d impurities. Amorphous alloys have a relatively flat optical reflectivity profile over the entire wavelength. We have used the free-electron model to study the relationship between optical reflectance at near-infrared wavelengths and transport properties of the Al-Ti alloys according to Eq. (3). We assume that the magnetic permeability is constant for non-ferromagnetic materials, such as pure Al and Ti, and does not vary significantly over the studied composition range. Aluminum alloys with dilute concentration of Cr, Mn, or Fe were found to be magnetic but non-magnetic in case of Ti. The optical reflectance depends mainly on the electrical resistivity ($\rho$) and the electron

### Table I. List of investigated sputter-deposited Ti, Al, and Al-Ti thin films showing the results from XRD, EXAFS, resistivity, and optical reflectance.

<table>
<thead>
<tr>
<th>Films composition</th>
<th>Crystal structure</th>
<th>NN</th>
<th>Interatomic distance R (Å)</th>
<th>$\sigma_0^2$ (Å$^{-2}$)</th>
<th>Resistivity ($\mu\Omega \times \text{cm}$)</th>
<th>Optical reflectance at 980 nm</th>
</tr>
</thead>
<tbody>
<tr>
<td>Al$_98$Ti$_2$</td>
<td>Polycrystalline</td>
<td>3.5</td>
<td>2.78 ± 0.014</td>
<td>0.010 ± 0.002</td>
<td>32</td>
<td>0.85</td>
</tr>
<tr>
<td>Al$_93$Ti$_7$</td>
<td>Polycrystalline</td>
<td>4</td>
<td>2.79 ± 0.01</td>
<td>0.008 ± 0.001</td>
<td>66</td>
<td>0.82</td>
</tr>
<tr>
<td>Al$<em>90$Ti$</em>{10}$</td>
<td>Polycrystalline</td>
<td>4.5</td>
<td>2.80 ± 0.007</td>
<td>0.0078 ± 0.001</td>
<td>70</td>
<td>0.69</td>
</tr>
<tr>
<td>Al$<em>93$Ti$</em>{15}$</td>
<td>Polycrystalline</td>
<td>5.3</td>
<td>2.80 ± 0.005</td>
<td>0.007 ± 0.001</td>
<td>91</td>
<td>0.64</td>
</tr>
<tr>
<td>Al$<em>90$Ti$</em>{20}$</td>
<td>Polycrystalline</td>
<td>5.1</td>
<td>2.82 ± 0.014</td>
<td>0.003 ± 0.002</td>
<td>121</td>
<td>0.62</td>
</tr>
<tr>
<td>Al$_96$Ti$_4$</td>
<td>Amorphous</td>
<td>3.9</td>
<td>2.75 ± 0.006</td>
<td>0.016 ± 0.012</td>
<td>186</td>
<td>0.6</td>
</tr>
<tr>
<td>Al$<em>96$Ti$</em>{10}$</td>
<td>Amorphous</td>
<td>3.04</td>
<td>2.76 ± 0.029</td>
<td>0.018 ± 0.005</td>
<td>219</td>
<td>0.55</td>
</tr>
<tr>
<td>Al$<em>96$Ti$</em>{16}$</td>
<td>Amorphous</td>
<td>2.43</td>
<td>2.74 ± 0.034</td>
<td>0.017 ± 0.006</td>
<td>278</td>
<td>0.52</td>
</tr>
<tr>
<td>Sputter deposited Al</td>
<td>...</td>
<td>...</td>
<td>...</td>
<td>...</td>
<td>...</td>
<td>0.69</td>
</tr>
<tr>
<td>Sputter deposited Ti</td>
<td>...</td>
<td>...</td>
<td>...</td>
<td>...</td>
<td>...</td>
<td>0.88</td>
</tr>
</tbody>
</table>

**FIG. 3.** Electrical resistivity of the sputter-deposited Al, Ti, and Al-Ti films with Ti content varying from 2% to 46%.

**FIG. 4.** Spectrally resolved total reflectance of poly-crystalline and amorphous Al-Ti alloys. Inset: optical intraband transition in sputter-deposited Al, 2% and 5% Ti-alloyed Al films.
scattering time (τ). Optical reflectance of the Al-Ti alloys as a function of the square root of the electrical resistivity is plotted in Fig. 5. The data are also given in Table I. The wavelength of 980 nm was chosen as it corresponds to a region where the reflectivity reaches a nearly steady state regime. It is worthwhile mentioning that at near infrared wavelengths, \( n \sim k \) for pure Ti and \( n \ll k \) for pure Al.\(^{27}\) Obviously, there will be a limit for which the Al-Ti alloyed system can satisfy Eq. (3). The data in Fig. 5 include pure Al, polycrystalline, and amorphous Al-Ti alloys. Note that pure Ti does not satisfy Eq. (3). Polycrystalline Al-Ti alloys have a high fraction of grain boundaries that increases with smaller grains, and thus it is expected to have a larger electrical resistivity compared to pure Al. Amorphous Al-Ti films have a larger offset compared to their polycrystalline counterpart, while their transport properties are governed by scattering of conduction electrons (anti-site effects and vacancies). EXAFS data indicate that amorphous alloys with large Ti content (Al\(_{64}\)Ti\(_{36}\) and Al\(_{53}\)Ti\(_{46}\)) have a more pronounced covalently bonded environment. Strong hybridization between sp-d electron states leads to a lower free electron density.\(^{28}\) Consequently, the Drude electron model was only used to describe the linear dependence between the optical reflectance and the square root of the electrical resistivity according to the classical reflection theory.

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FIG. 5. Optical reflectivity of the crystalline and amorphous Al-Ti alloys at 980 nm as a function of square root of the electrical resistivity. The linear fit of the reflectivity \( R \) versus \( \rho^{1/2} \) corresponds to the polycrystalline alloys with Ti content varying from 2% to 20%.

27M. N. Polyaniskiy, Refractive index database, 2016.